Regularities in Variation of Support Functions of Physically Nonlinear Elastic-Visco-Plastic Law of Strain of Cotton Yarn

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Abstract
Support functions of the parameters variation of proposed physically nonlinear elastic-visco-plastic law of strain of cotton yarn are determined on the basis of the results of processing the experimental data on yarn tension to breakage. These functions allow us to determine the average values of nonlinear law parameters, which allow its use in practice in solving the applied problems of yarn mechanics and determining and evaluating the strength of cotton yarn.

Keywords
Cotton yarn; Nonlinear law; Variable modulus of strain; Parameters of modulus change; Experiment; Yarn strength; Linear density of yarn

Problem Statement
On the basis of fundamental concepts [1-3] and principles of the mechanics of structurally unsteady bodies and media under strain [4-7], a physically nonlinear elastic-visco-plastic law of strain of cotton yarn under tension to breakage was proposed [8]. Taking into account the unloading, this law takes the following form.

\[ E_0(\varepsilon) \frac{d\sigma}{dt} + E_e(\varepsilon) \sigma = \frac{de}{dt} + \mu(\varepsilon) \varepsilon \] \[ E_m(\varepsilon) \frac{d\sigma}{dt} = \frac{de}{dt} \] or

\[ E_s(\varepsilon) \] \[ E_k(\varepsilon) \frac{d\sigma}{dt} = \frac{de}{dt} \] or

where \( \sigma \) is a longitudinal tensile stress, \( t \) — a longitudinal strain of yarn, \( t \) — time.

A nonlinear function \( E_e(\varepsilon) \) a quasi-static modulus of strain under cotton yarn tension is defined. The methods for determining \( E_e(\varepsilon) \) a function of dynamic strain modulus, \( \mu(\varepsilon) \) a function of viscosity parameter, \( E_s(\varepsilon) \) a function of unloading modulus are also considered [8]. Strain law (1) is developed on the basis of a linear viscoelastic model of a standard linear body.

It was shown in [8] that the nonlinear function of the change in modulus of cotton yarn strain \( E_e(\varepsilon) \) has the following parameters: \( E_N \)

is an initial value at \( \varepsilon = \varepsilon_0 = 0 \); \( E_i \) is a minimum value at \( \varepsilon = \varepsilon_i \); \( E_m \) is a maximum value at \( \varepsilon = \varepsilon_m \); \( E_k \) is a critical value of the strain modulus at \( \varepsilon = \varepsilon_k \) at the moment of yarn breakage. Here a value of strain modulus in the interval \( [\varepsilon_e, \varepsilon_k] \), denoted by \( E_i \), has also been introduced. The point is that strain modulus in the interval \( [\varepsilon_e, \varepsilon_k] \) is always decreasing. In some cases, after reaching the value \( E_s(\varepsilon) \) with further rise in strain, the decline of \( E \) ceases, and remains approximately constant or increases. This moment at \( \varepsilon = \varepsilon_k \) and \( E = E_k \) is fixed as an additional point. Behind this point, the value of \( E \) either continues to decrease or remains constant, or increases.

Thus, the parameters of strain modulus \( E(\varepsilon) \) variation under yarn tension to breakage are \( E_N, E_e, E_m, E_k, E_t, E_{\varepsilon_0}, E_{\varepsilon_i}, E_{\varepsilon_m}, E_{\varepsilon_k} \). The values of these parameters depend on linear density of cotton yarn as the results of experiments show [8]. The aim of this work is to determine the dependence of these parameters on linear density of cotton yarn.

Determination of the Parameters of Strain Modulus

Experiments on cotton yarn tension to breakage were carried out with the nominal linear densities: \( T = 14.0 \) tex; 15.4 (2); 16.5 (2); 18.5 (5); 29.0 (16); 50.0 (10); 72.0 (4); 100.0 (3); 160.0 (1) tex [8]. The number of spoons with given linear density is indicated in parentheses. A total of 45 spoons were produced. Before the test, as noted in [8], linear density of the yarn for each spoon was determined separately [8]. As a result, actual linear densities of the yarn in each of the 45 spoons [8] were obtained, which are given below.

For given nominal density \( T = 14.0 \) tex: 14.56 and 14.6 tex; for \( T = 15.4 \) tex: 14.7 and 15.0 tex; for \( T = 16.5 \) tex: 16.7 and 16.9 tex; for \( T = 18.5 \) tex: 17.73; 18.41; 18.6; 19.2 and 20.2 tex; for \( T = 29.0 \) tex: 27.7; 28.10; 28.30; 28.50; 28.52; 28.61; 28.63; 28.7; 28.96; 29.03; 29.1; 29.27; 29.4; 29.5; 29.56 and 31.3 tex; for \( T = 50.0 \) tex: 48.18; 48.2; 48.54; 49.10; 49.16; 49.32; 49.8; 50.03; 50.02 and 50.7 tex; for \( T = 72.0 \) tex: 70.68; 71.41; 71.21 and 71.42 tex; for \( T = 100.0 \) tex: 97.36; 97.4; 102.76 tex and \( T = 162.13 \) tex.

Cotton yarns from each spoon were tested on the «Statimat C» device consistently for 50 times, i.e. the experiment is repeated for 50 times. Then, the obtained 50 dependences of tensile force \( F \) versus strain \( \varepsilon \) (%) are averaged by the software installed in the device. From the obtained average dependence \( F(\varepsilon) \) we determine the change in strain modulus \( E(\varepsilon) \) by the method described [8]. From each dependence \( E(\varepsilon) \) (total number of dependences \( E(\varepsilon) = 45 \)), the values of parameters \( E_N, E_e, E_m, E_k, E_t, E_{\varepsilon_0}, E_{\varepsilon_i}, E_{\varepsilon_m}, E_{\varepsilon_k} \) in MPa and \( \varepsilon_e, \varepsilon_i, \varepsilon_m, \varepsilon_k \) in dimensionless form were determined according to the method described in [8]. The value of \( E_N \) is taken equal to zero (\( \varepsilon_e = 0 \)).

Figure 1 shows the changes in initial values of strain modulus \( E_N \) in MPa, depending on the actual linear density \( T \) in tex (1 tex = 10⁻³ N/m), based on experimental data (curve 1). Here, linear density of cotton yarn \( T \) corresponds to the actual measured value before the experiment for each yarn spoon.

As seen from Figure 1, the change in actual initial values \( E_N \) at different actual values of \( T \) (curve 1) has a significant scattering.

The general trend of change in curve 1, Figure 1, is decreased with increased \( T \). However, the very stochastic change in functions \( T \) and \( E_N(T) \) according to curve 1, Figure 1, could not be described analytically.
so this curve was averaged over the nominal values of linear densities of cotton yarn. At the same time, close values of nominal linear densities were also combined into one group. As a result, the following six groups of linear densities were obtained.

The first group includes the yarns related to the nominal linear densities of \( T = 14.0 \), 15.4; 16.5; 18.5 tex. The second group consists of yarns related to \( T = 29.0 \) tex. The third group includes the yarns related to \( T = 50.0 \) tex. The fourth group includes the yarns related to \( T = 72.0 \) tex. The fifth group includes the yarns related to \( T = 100.0 \) tex and the sixth group consists of yarns with \( T = 160.0 \) tex. For each group, the values of linear density and the parameters \( E_{N_1}, E_{N_2}, E_{N_3}, E_{m}, e_N, e_e, e_m, \epsilon_N, \epsilon_e \) and \( \epsilon_m \) were also averaged.

Curve 2, Figure 1, was obtained using the averaged values of \( T \) and \( E_e \) for six groups. As seen from Figure 1 (curve 2), the change in mean values of \( E_e \) for \( T \) groups has already some explainable pattern of variation with increasing linear density of yarn. For small values of \( T \), the initial value of strain modulus \( E_1 \) is the greatest, and then the value of \( E_1 \) decreases with increasing \( T \). At nominal values of \( T = 100.0 \) and 162.0 tex, a slight increase in value \( E_1 \) was observed. Now, curve 2, Figure 1, can be approximated by an analytic function. To do this, we choose a decreasing power function in the form

\[
E_N(t) = E_{N1} \left( \frac{T}{T_1} \right)^{\chi_1},
\]

Where \( E_{N1}, T_1 \) and \( E_{N1}, T_2 \) and \( \chi_1 \) are the coefficients of function (3), which must be determined. The ratio \( T/T_1 \) is taken in order to have a dimensionless value in parenthesis in relationship (3). With the value of \( T_1 = 50.0 \) tex, in most cases the values of dependence parameters \( E(t) \) become steady or increasing.

The remaining two parameters of formula (3) \( E_{N1} \) and \( \chi_1 \) are determined by the method of least squares on a computer, and they are: \( E_{N1} = 2872.944 \text{ MPa} \) and \( \chi_1 = -0.302174 \). Here \( \chi_1 \) is a dimensionless quantity. Curve 3, Figure 1, is constructed using formula (3).

The change in strain modulus \( E_e \) with increasing linear density of cotton yarn \( T \), according to curve 3 (dotted curve), Figure 1, occurs monotonically, without any leaps. Thus, with certain transformations and averaging of curve 1 (Figure 1), obtained as a result of processing the results of the experiments, we obtain curve 3, which already indicates a certain pattern of change in the strain modulus \( E_e \) at different values of linear density of cotton yarn \( T \).

With increasing linear density of cotton yarn \( T \) the value of strain modulus \( E_e \) gradually decreases. This statement, in general, does not contradict the results given in [1-3]. Using formula (3), it is possible to determine the value of strain modulus \( E_e \) for any value of linear density of the yarn obtained by pneumatic-mechanical method of card system spinning.

Figure 2 shows the change in the second parameter \( E(\varepsilon) \), of the minimum value of strain modulus \( E_m \) in MPa, depending on linear density of cotton yarn.

Here, as in Figure 1, curve 1 – is a variation in actual values of \( E_m \) depending on actual values of linear density of the yarn \( T \). Curve 2 – is a variation in averaged values of \( E_m \) depending on averaged values of actual values of \( T \). As seen from Figure 2 (curve 2), the value of \( E_m \) with increasing linear density of the yarn sharply decreases to the value of \( T_0 = 50.0 \) tex, while at \( T > 50.0 \) tex its decrease is not so intensive.

Approximate curve 2 (Figure 2) with power function in the form

\[
E_m(T) = E_{m1} \left( \frac{T}{T_1} \right)^{\chi_1},
\]

The coefficients \( E_{m1} = 1274.765 \text{ MPa} \) and \( \chi_2 = -0.544665 \) are determined by the method of least squares.

Curve 3, Figure 2, is constructed using formula (4). This curve is already a monotonically decreasing function of \( E_m \), depending on the value of linear density of the yarn \( T \).

Figure 3 shows similar variations in the parameter of \( E_{N1} – \) the maximum value of strain modulus of cotton yarn versus linear density of the yarn \( T \).

Here, curve 1 is a variation in actual values of \( E_{N1} \) depending on actual values of linear density. Curve 2 is constructed from average values of \( E_{N1} \) and \( T \) by groups of linear densities of yarn.

Variations in the maximum average value of strain modulus \( E_{N1} \) depending on averaged values of linear density of the yarn (curve 2, Figure 3), change in a more complicated way. To describe this curve, a power function is taken in the form

\[
E_{N1}(T) = E_{N1} \left( \frac{T}{T_1} \right)^{\chi_1},
\]
Here, the values of coefficients $E_{mk} = 2705.089$ MPa and $X_1 = -0.202455$ are determined by the method of least squares. Here, $T_\nu$ = 50.0 tex. At linear density from 10 tex to 160 tex, in 10 tex steps, the value of $E_\nu$ is calculated and curve 3 is obtained according to formula (5) (Figure 3).

Curve 3 is actually an approximating curve 2 (Figure 3) and according to formula (5) the value of $E_\nu$ as well as $E_\nu$ and $E_s$ (Figures 1 and 2) decreases monotonically with increasing linear density of yarn $T$.

Figure 4 shows the variations in the actual (curve 1), averaged (curve 2) and approximating (curve 3) values of strain modulus $E_s$ (intermediate between $E_m$ and $E_k$), depending on the values of linear density of cotton yarn $T$.

Curve 3 is obtained with formula

$$E_s(T) = E_{mk} \left( \frac{T}{T_s} \right)^{\chi_s},$$  

where $E_{mk} = 2579.042$ MPa and $X_1 = -0.141952$ both quantities are determined by the method of least squares using the averaged values of $E_s$ and $T$ by groups of linear densities.

Figure 5 shows similar changes in the critical strain modulus $E_k$ reached before the breakage of cotton yarn, depending on its linear density. Here, too, curve 1 is plotted by actual values of $E_k$ and $T$; curve 2 is plotted by averaged values of $E_k$ and $T$.

Curve 3 is obtained with formula

$$E_k(T) = E_{mk} \left( \frac{T}{T_s} \right)^{\chi_k},$$  

The values of coefficients $E_{mk} = 2222.351$ MPa and $X_1 = -0.365873$ are determined using the least squares method. Here $T_\nu$ = 50.0 tex.

The nature of variations in actual, averaged and approximate curves $E_k(T)$ (curves 1-3, Figure 5) is similar to the changes in $E_s$, $E_m$, $E_e$, and $E_s$ depending on the values of linear density of cotton yarn $T$.

Thus, the change in the parameters of functions of strain modulus $E(\varepsilon)$, initial modulus $E_s$, minimum modulus $E_m$, maximum modulus $E_k$, intermediate modulus $E_e$, and critical modulus $E_k$ are determined on the basis of the results of processing experiments on cotton yarn tension to breakage [8].

The nature of the change in functions $E_s(T)$, $E_m(T)$, $E_e(T)$, and $E_k(T)$ according to Figures 1-5 is approximately the same: they generally decrease with increasing linear density of cotton yarn.

Formulas (3)-(7) allow us to determine by calculation the values of $E_s$, $E_m$, $E_e$, and $E_k$ for any values of linear density of yarn $T$. The obtained values of strain modulus $E_s$, $E_m$, $E_e$, $E_k$, and $E_k$ correspond to a certain average value of these modules for cotton yarns with linear density $T$ of the card system produced by pneu-mechanical spinning. For other systems and spinning methods, these parameters must be determined from the results of corresponding experiments on yarn tension to breakage.

**Determination of Strain Parameters**

Strain parameters of the function of modulus change $E(\varepsilon)$, are $\varepsilon_m$, $\varepsilon_e$, $\varepsilon_m$, $\varepsilon_e$, and $\varepsilon_k$. Initial value of strain modulus of cotton yarn $E_{\varepsilon_i}$ from dependence $E(\varepsilon)$, obtained from experimental results, was determined at $\varepsilon_{\varepsilon_0} = 0.00025$, i.e. very close to zero. Therefore, the value of $\varepsilon_{\varepsilon_0}$ in all cases is assumed to be zero, i.e. $\varepsilon_{\varepsilon_0} = 0$. In fact, $E_{\varepsilon_i}$ is a strain modulus of non-deformable cotton yarn at $\varepsilon_{\varepsilon_0} = 0$. But the value of $E_{\varepsilon_i}$ at $\varepsilon_{\varepsilon_0} = 0$ cannot be determined. Therefore, in the determination of modulus $E_{\varepsilon_i}$, the strain value is taken very close to zero. Consider the change in remaining strain parameters of dependence $E(\varepsilon)$, versus linear density of cotton yarn.
Figure 6 shows the dependence of $\varepsilon_e$, when strain modulus $E$ reaches the value of $E_e$, on linear density of cotton yarn. Here, curve 1 is plotted according to actual values $\varepsilon_e$ and $T$, i.e. it shows an actual change in parameter $\varepsilon_e$ from the actual values of linear density of the yarn used in experiments.

As seen from Figure 6, the change in curve 1 is chaotic and does not yield to any analytical description. Having the average values of $\varepsilon_e$ and $T$ by groups of linear densities of cotton yarn, curve 2 is obtained. From the character of curve 2, it can be stated that with increasing linear density of yarn, the value of $\varepsilon_e$ tends to increase. It is possible to analytically describe curve 2 by a more complicated function. However, for simplicity, it is approximated by a linear function in the form

$$\varepsilon_e(T) = a_e + b_e T,$$

where $a_e = 0.000321$; $b_e = 0.000034$ tex$^{-1}$, determined by the method of least squares on the basis of dependence (8). Straight line 3 in Figure 6 is constructed using formula (8), setting a value of $T$ from zero to 160 tex, in 10 tex steps. As seen from Figure 6, line 3 is actually the average straight line for curve 2.

Figure 7 shows the changes in strain parameter $\varepsilon_m$, at which strain modulus of the yarn $E$ reaches its maximum value $E_m$, depending on the values of linear density of cotton yarn $T$.

Here, too, curve 1 is an actual change of $\varepsilon_m$ versus actual value of $T$. Curve 2 is the change in average values of $\varepsilon_m$ and $T$ by groups of linear densities.

Curve 3 in Figure 7 is an approximation of curve 2, just as in the previous case, by a straight line in the form

$$\varepsilon_m(T) = a_m + b_m T,$$

where $a_m = 0.006054$; $b_m = 0.000125$ tex$^{-1}$ – are the coefficients whose values are determined by the method of least squares.

Figure 8 shows the dependencies $\varepsilon_S(T)$ obtained by processing the results of experiments.

Curve 1 is obtained on the basis of actual values $\varepsilon_S$ with actual values of linear densities.

Curve 2 is constructed on the basis of average values $\varepsilon_S$ and $T$ by groups of linear densities. Curve 3 in Figure 8 is an approximation of curve 2, just as in the previous case, by a straight line in the form

$$\varepsilon_S(T) = a_S + b_S T,$$

Where $a_S = 0.022211$; $b_S = 0.000235$ tex$^{-1}$ – are the coefficients determined using the least squares method.

The change in critical value of strain $\varepsilon_k$ at the moment of cotton yarn breakage versus linear density of the yarn is shown in Figure 9.

Here, too, curve 1 describes the change in critical strain $\varepsilon_k$ versus
actual linear density of the yarn. As seen from Figure 9, this curve also changes in a complex, stochastic manner.

Curve 2 in Figure 9 is constructed from the average data values of \( \epsilon_2 \) and \( T \) by groups of linear densities.

Certain regularity is already observed in the character of the change in curve 2 (Figure 9). This curve is also approximated by a linear function in the form

\[
e(\epsilon) = a + b\epsilon,
\]

where the values of \( a \) and \( b \) are determined by the method of least squares and they are: \( a = 0.056204; b = 0.000453 \) tex\(^{-1}\).

As seen from Figure 9, the straight line 3, constructed according to formula (11), describes the curve 2 with satisfactory accuracy. The value of critical strain \( \epsilon_k \) for cotton yarn with certain linear density is considered constant. For different values of linear density the values of \( \epsilon_k \) are determined using formula (11).

Thus, the specific values of the parameters of functions \( E(\epsilon)-E_N, \epsilon_N, \epsilon_e, \epsilon_m, \epsilon_S, \epsilon_k \), for specific values of linear densities of cotton yarn \( T \), are determined from equations (3) - (11).

With known values of these parameters, according to the procedure given [8], the change in strain modulus for cotton yarn with specific linear density \( T \), is approximated versus the values of longitudinal strain \( \epsilon \) under yarn tension to breakage.

As was noted above, equations (3) - (11) are valid only for cotton yarn of a carded spinning system produced on a pneumatic-mechanical spinning machine from medium-fiber cotton of the 1st grade, of the 1st group of maturity, of the 4th type of fiber [8]. For yarns obtained by other technological methods and from other types of cotton, the values of function parameters \( E(\epsilon) \) and equations (3) - (11) should be re-established according to the results of experiments on stretching these yarns to breakage and from the results of their processing.

The physically nonlinear elastic-viscoplastic law (1) [8], describing the process of strain of cotton yarn to breakage, includes functional parameters \( E_N, E_e, E_m, E_S, \epsilon_N, \epsilon_e, \epsilon_m, \epsilon_S, \epsilon_k \) and \( \mu(\epsilon) \). The function of quasistatic change of cotton yarn strain modulus \( E(\epsilon) \) includes parameters \( E_N, E_e, E_m, E_s, \epsilon_N, \epsilon_e, \epsilon_m, \epsilon_S, \epsilon_k \) and \( \epsilon_0 \). The values of these parameters are determined from equations (3) - (11). The function of dynamic strain modulus \( E_D(\epsilon) \) is determined through the relation \( E_D(\epsilon)=yE(\epsilon) \). As stated in [8], value of \( y \), for cotton yarn varies from 1.1 to 4. The current value of \( y \), the function of viscosity parameter \( \mu(\epsilon) \) and the unloading function \( E(\epsilon) \) were determined from the relations proposed [8]. The unloading functions must be determined from the results of the corresponding experiments.

Thus, all functional parameters of the nonlinear law (1) and (2) become approximately known. This allows us to use the proposed law in applied problems of mechanics of yarns and in evaluating and predicting the strength of cotton yarn.

Conclusion

1. Based on the analysis of processing results of experiments on cotton yarn stretching, functional parameters in the parameters of quasi-static modulus of yarn strain \( E(\epsilon) \) are determined versus the values of linear density of cotton yarn.

2. The proposed functional relationships describing the changes in parameters \( E_N, E_e, E_m, E_s, \epsilon_N, \epsilon_e, \epsilon_m, \epsilon_S, \epsilon_k \) and \( \epsilon_0 \) depending on linear density of cotton yarn. This makes it possible to use the proposed nonlinear law of cotton yarn strain in applied problems of mechanics of textile yarns and threads.

3. Based on the proposed methods, it is possible to determine the functional parameters of the proposed nonlinear law for various types of yarns and textile threads and to assess the applicability of the proposed law under tension of these materials; this is a challenge for the future.

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References