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## **Research Article**

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## Assessing the Lateral Erosion of Main Meandering Rivers in the Mid-Central Part of Vietnam

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#### Abstract

Until now, predicted methods of lateral erosion of rivers have been not much, especially that are still have not been completed any scientific base. Nonetheless that the article try to test and apply the method of power equilibrium (semi-empirical method) to assess the lateral eroded rate of the mid-downstream of main rivers in the midcentral part of Vietnam as Gianh River, Nhat Le River, Thach Han River, Huong River, Thu Bon River, Tra Khuc River and Ba River. Through research results, they show of almost rivers have the rate of lateral erosion alternated from moderate (2-5 m/year) to strong (5-10 m/year). In particularly, Nhat Le River where commonly weak lateral erosion (<2 m/year) occurs. In addition, the erosion activity are strongly differentiated by space-time and completely depends on the morphological characteristics of river channel, soil composition and ground structure of riverbanks and hydrology - hydraulic regime of each river section. These gathered results are suitable for our field investigation for the in research rivers in period 2012-2015. We propose applying method for wide alluvial anabranching rivers in the mid-central part of Vietnam.

#### Keywords

Lateral erosion; Riverbank; Hickins E.J-Nanson G.C; Eroded rate

## Introduction

As for present situation in Vietnam as well as the world, in order to predict the lateral erosion, there are various methods applied differently, generally, they have divided into 3 main method groups: Actual state assessment with remote sensing image analysis; Lateral erosion calculating by the semi-empirical method and Physic-Mathematic models.

Besides, Common characteristics of the mid-central rivers of Vietnam are slope, short, meander and near the highly dissected mountains where are oriented from the Northwest to Southeast that lead to the high rainfall. Additionally, the structures of riverbanks consist of the mixture of mud, cohesive - granular soils. Thus, under the impact of bed forming discharge and economic- engineering activities, the lateral erosion process of the investigated rivers occur regularly annually causing serious impacts on the environment of the study area [1,2].

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Therefore, this research shows several results of our investigation on the erosion degree of main rivers (including Gianh, Nhat Le, Thach Han, Huong, Thu Bon, Tra Khuc and Ba Rivers) located in the mid-central part of Vietnam, which prolongs from Quang Binh to Phu Yen province (Figure 1). Lateral erosion occurs frequently in the region of interest when flood season comes, causes serious losses of infrastructure, livelihood, economy-society, security-defense and ecological environment. In term of nature, hydrodynamic pressure is the main cause of erosion activities, especially the flood flows, shown through deep erosion and lateral erosion, which effect negatively on the environment. In addition, they also cause the non-stability of construction as well as planning of socio-economic sustainable development. However, lateral erosion usually influence to building planning, residential distribution at two riversides. At present, the research and propose assessment and prediction methods for river channel changes in generally, the lateral erosion in particularly are not numerous and still do not meet the necessary reliability. By facing this situation that there are many negative changes which occurs in river channel, there are several researches who worked on river erosion activities in the mid central part of Vietnam from the historical flood in 1999 up to now such as: Anh [3], Dan [4], Tho and Thanh [5], Thien [1,6-14], Van [15], Yem [16], etc. In addition, there are a number of other published researches have been carried out by us in study area for recent [2,12-14]. However, there are few researches, which apply semi-empirical expression for the prediction of lateral erosion in Vietnam Rivers [2,13,17,18].

In the last decades, the semi-empirical methods were applied in wide range to predict the lateral erosion of riverbanks in the world. Several typical researches as following:

1. Brice [19] measured river erosion on a study group of 36 streams, which indicate that channel instability is manifested by lateral bank erosion. Lateral stability is related to four major stream types (equi-width, wide-bend point bar, braided point-bar, and braided) with equi-width streams have the lowest erosion rates and braided point-bar streams the highest, erosion rates (V) increase associated stream size (B) following the empirical function:

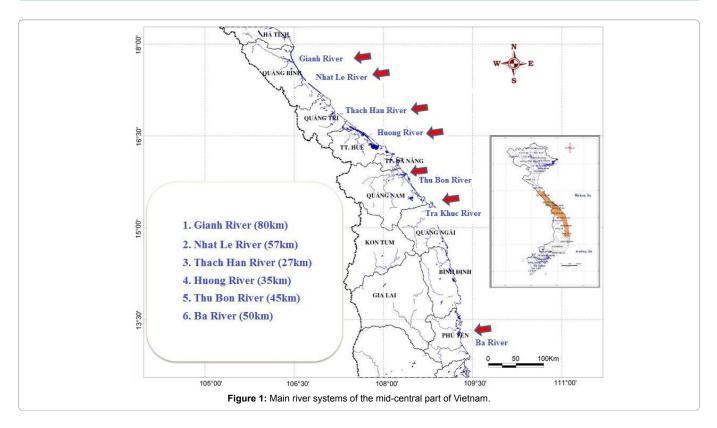
2. Hooke [20] proposed that the erosion rate (V) is most closely related to catchment area (A) as a surrogate of discharge and width. Rates of bank erosion were determined from field measurements and historical maps for 11 streams in Devon, England. Then the rates of bank erosion were compared with worldwide published rates in 43 streams. The equation was derived through multiple regression analysis using the 54 data points and resulted in very high rates of bank erosion. The equation was then modified with the same data from 11 streams in Devon, England and 43 streams from literature, given as follows:

$$V = 0.0669 A^{0.46}$$
(2)

3. Keady and Priest [21] obtained the data to develop the equation was from the following rivers: Mississippi River; Red River; Pearl River; Tombigbee River; Buffalo River; Red Deer River (Canada). The influencing parameters found by those authors are the slope of the river (s) and the amplitude of meander (A). Other

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variables involved in the equation are the gravity (g) and a function of the slope ( $\phi(s)$ ). The relation shown in the following equation:

$$\frac{V}{\sqrt{(gA)}} = \emptyset \tag{3}$$

In which: V (ft/y)=migration rate=dM/dt; g (ft/s)=acceleration of gravity; A (ft)=meander amplitude; S=slope; f (s)=f (s)=function of s.

4. Odgaard [22] solved constitutive equations by assuming that the rate of bank erosion is proportional to the difference between the near-bank depth-averaged mean velocity and the reach-averaged mean velocity at bank full discharge. The resulted equation indicates that the erosion rate is correlated with channel characteristics such as width, depth, curvature, bend angle of channel centerline, channel slope, friction factor, and degree of vegetation on the banks. The predictions using this equation agreed well with data measured by using historical records (air photos, maps, and stream flow records), field measurements, and soil analysis in East Nishnabotna River and Des Moines River in Iowa.

$$\frac{v}{u} = 2E \frac{b}{r_c} (1 + \frac{b}{2r_c})^{-1} F$$
(4)

$$F = 1 - \exp\left[-B\frac{r_c\phi}{b}(1 - \frac{\beta}{\phi})\right]$$
(5)

$$F = 1 - \exp\left[-B\frac{r_c\phi}{b}(1 - \frac{\beta}{\phi})\right] \tag{6}$$

$$B = \frac{2k^2 \ b}{(m+1)^2 \ d_c}$$
(7)

Where,

v (m/year): the average rate of erosion; u (m/s): reach-average

mean velocity; e: erosion constant;  $\alpha$ : 1.27;  $\theta$ : Shields' parameter, 0.06; m: friction parameter; k: Karman's constant, 0.40; F: particle Froude number; b (m): bank-full width of channel; r (m): radius of curvature.  $\varphi$ : bend angle;  $\beta$ : angle from cross over to first outer bank erosion occurrence; d: centerline flow depth. In the calculations, two variables were assumed for this study: the friction factor (m) was taken as 3 and particle Froude number  $(F_{D_c})$  [22]. In addition, the erosion constant was taken as  $e=6.4 \times 10^{-7}$  and  $e=4.4 \times 10^{-7}$  for the case of light or no vegetation and dense vegetation on outer bank, respectively. This method considers flow (u), soils (e), and geometry (b/r). If the right erosion constant was picked, the predicted migration rate is close to the measured one. Although soil erosion is a fundamental property of soils, it was treated as an empirical coefficient here. A value can be chosen based on existing records. But there is no guarantee that the value will work for a true prediction case. The erosion resistance of soils can be obtained by using EFA (Erosion Function Apparatus) to test the erosion function of soil [23]. It is worthwhile to study how to replace erosion constant e here with EFA function. The above method was a simplified version of a more complex solution developed by the same author Odgaard [22]. A modified version came out soon. However, unfortunately the answer was very sensitive to some parameters.

Additionally, there are also a number of other researches, which mention to the prediction of meander migration by computer programs and be also widely cited in literatures as Wang [24], Thien [11-14,16].

Nonetheless, above methods are simple determine the qualitatively rather than quantitatively. As well as they mention incompletely to the parameters of river hydro-morphology, lead to the great difference existence between calculating results and field measuring for Vietnam meander rivers in generally and the mid-central part

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of Vietnam in particularly, whose riverbanks are structured by the organic mud, cohesive soils, granular soils and gravels. Meanwhile, calculating the lateral erosion rate by the method of Hickins and Nanson [25] in some Vietnam Rivers are reliable and consistent with the investigated data [5,7,8,12-14]. Therefore, we utilize the above semi-empirical method to assess the lateral eroded rate in the region of interest, to orient for reasonable prevention science and technology solutions to mitigate the serious damages by the process of erosion caused, attained to the suitable exploitation and geological environmental protection of the territory. Simultaneously, determine the erosion belts for the planning and development of industrial and residential zones.

#### **Base documents**

To implement calculating and predicting the rate of lateral erosion of above rivers, the authors use data and documents as below [7,11,12-15] (Figures 2 and 3):

1. The geological and topographical features, the erosion resistance (Monogram of Hickins and Nanson [25]), structure and lithological composition of rocks and soils created the riverbanks, riverbank elevation at hydro-morphological cross-sections, the width of flows or channels, bend radius of meandering bank and so on.



Figure 2: Measure hydro-morphological characteristics of Vietnam mid-central rivers (a) The bottom sediment sampling, (b) Granular composition test, (c,d) Measure hydrological cross section.



Figure 3: Investigate the actuality of erosion and erosion preventive measures, mitigation of damages for Vietnam mid-central rivers (a) Riverbank erosion investigation, (b) Sediment sampling at riverbanks, (c,d) Investigate erosion prevention works

2. The hydrological characteristics at 15 cross sections in Gianh River, 12 sections in Nhat Le River, 8 sections in Thach Han River, 5 sections in Huong River, 9 sections in Thu Bon River, 6 sections in Tra Khuc River and 5 sections Ba River was calculated as bed forming discharge  $(Q_{cf})$ , the average depth of flood flow, the hydraulic slope of flow  $(J_{cf})$  in the investigated rivers (Figures 4-8).

The results of state investigation of lateral erosion after flood season in period 2012-2015 combine with state report of riverbank and estuary erosion from Storm and Flood Control and Dyke Management of provinces in the mid-central part of Vietnam.

### **Research Methods**

Nanson and Hickin [26] described that the ratio of radius of curvature of a bend (R) to channel width (W) influences the lateral migration rate of a meandering river. The relationship between channel migration rate (MR) and the ratio of radius of curvature to channel width for the Beatton River, Canada and other rivers indicate that the normalized migration rate (MR/W) is highest when the ratio of radius of curvature to channel width (R<sub>c</sub>/W) is about 3. Their data confirm, approximately, the following relations:

MR=2.0 
$$(R_c/W)^{-1}$$
 for  $(R_c/W) \ge 31$  (9)

Where, MR (m/year): Mean Erosion Rate; W (m): Channel Width; R $_{\rm c}$ (m): Radius of Curvature

This relationship between migration rate and geometry was widely cited in literature. But the scatter in data doesn't necessarily lead to the relationship the authors proposed. With the same data, different persons may come up with completely different relationships. Geometry is only one factor affecting meander migration. Other important factors such as velocity and soil properties were ignored in the authors' conclusion. This study described the relation between migration rate and geometry qualitatively rather than quantitatively. Thus, these authors continued to complete above semi-empirical equation in research as specified [7]:

Based on the empirical research for the rate of lateral erosion in 189 riverbanks, it created from clayey and sandy soils of 21 rivers in West Canada. Later, these authors established the equilibrium equation between rate of lateral erosion M ( $R/B_{cf}$ ) with hydrodynamic pressure of flow, eroded resistance of rocks and soils at the riverbank; and the features of hydrology - morphology of flow. Finally, the empirical expression is a multivariate functions as follows.

$$M(\frac{R}{B_{cf}}) = f(\Omega_{cf}, \overline{S_{sb}}, \overline{H_{cf}}, R, B_{cf})$$
(10)

By dimensional analysis of variables and streamlining function under really situation, the authors gave the formulas to determine the rate of lateral erosion as below:

$$M(\frac{R}{B_{cf}}) = 2,5M_{2,5}(\frac{R}{B_{cf}})^{-1}, with \frac{R}{B_{cf}} > 2,5$$
 (11a)

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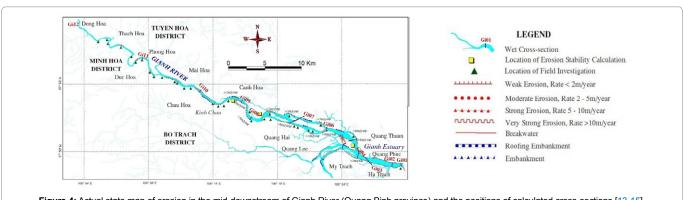


Figure 4: Actual state map of erosion in the mid-downstream of Gianh River (Quang Binh province) and the positions of calculated cross-sections [13-15].

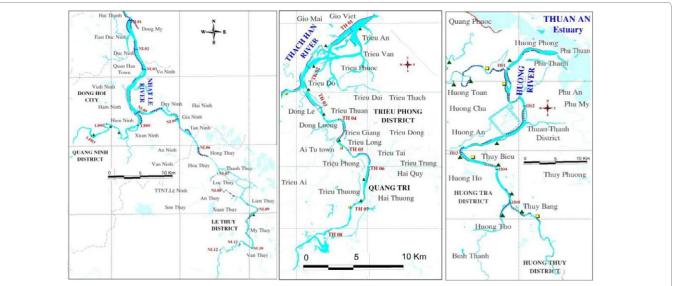
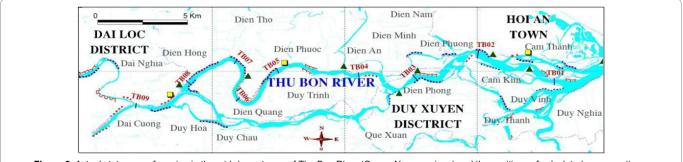


Figure 5: Actual state map of erosion in the mid-downstream of Nhat Le River (Quang Binh province), Thach Han River (Quang Tri province), Huong River (Thua Thien Hue province) and the positions of calculated cross-sections.





Or 
$$M(\frac{R}{B_{cf}}) = \frac{2}{3}M_{2,5}(\frac{R}{B_{cf}} - 1)$$
, with  $\frac{R}{B_{cf}} < 2,5$  (11b)

Where: 
$$M2,5 = \frac{\Omega_{cf}}{\overline{H_{cf}}.S_{sb}}$$
 (12)

$$\Omega_{cf} = \Delta w.g.J_{cf}.Q_{cf} \text{ N/m}$$
(13)

 $\Delta_{w}$ : Specific Gravity of Water (1000 kg/m<sup>3</sup>);

g: Acceleration of Gravity (9.81 m/s<sup>2</sup>);

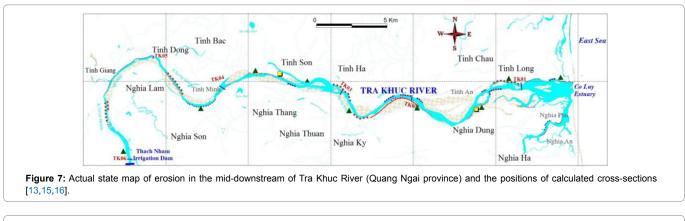
J<sub>cf</sub>: Hydraulic Slope along Flood Flow;

Q<sub>cf</sub>: Bed-Forming Discharge (m<sup>3</sup>/s).

#### **Research Results and Discussion**

In order to calculate rate of lateral erosion M (R/B<sub>cf</sub>) in middownstream of investigated rivers, we implement to determine hydro-morphology characteristics at the cross-sections. In which, the

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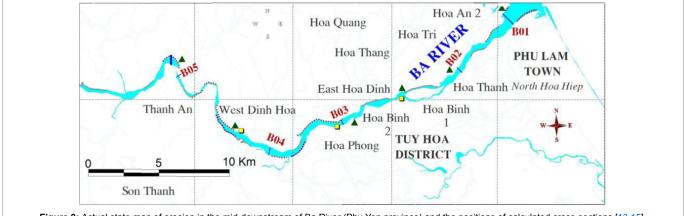


Figure 8: Actual state map of erosion in the mid-downstream of Ba River (Phu Yen province) and the positions of calculated cross-sections [13,15].

bed forming discharge  $(Q_{cf'} m^3/s)$  was identified by various following methods [24,27]:

As for river sections without hydrological station level 1 (monitor water levels, flows, sediment loads), we applied flood flow method when floods spread out the riverbank. Gianh River is an example in flood season in October, 2010 with  $Q_{cf}(1063 \text{ m}^3\text{/s})$  was identified at cross-section Gi15 (Kim Hoa commune); Also for Nhat Le River (in flood season September, 1968) with  $Q_{cf}$  (2110 m<sup>3</sup>/s) determined at cross-section NL12 [14]; As for Thach Han River,  $Q_{cf}(1750 \text{ m}^3/\text{s})$ was identified from monitoring data in flood season October, 2010 at cross-section TH08 (Tram dam) [3]. By Huong River and Thu Bon River, Q<sub>cf</sub> was identified from monitoring data of floods in October-November, 2000 at river cross-sections as H05 (Kim Long, 2550 m3/s), TB09 (Giao Thuy, 4350 m3/s), TB03 (Cau Lau, 3250 m3/s) [1,7,10-12]. In addition, the paper also utilizes data series in period 1979 - 2008 at Son Giang hydrological measuring station for Tra Khuc River and Cung Son station for Ba River, in combination with frequency method to guarantee about 5 percent accurate for Q<sub>cf</sub> (1400 m<sup>3</sup>/s) determination at river cross-section TK06 (downstream of Thach Nham dam) and the method of Makaveev to identify  $Q_{st}$  (2100 m<sup>3</sup>/s) at river cross-section B05 (Dong Cam dam) [13]. The calculated results of lateral erosion rate at cross- sections are shown in Tables 1-3 and Figure 9 as following:

1. Through Tables 1 and 2, they indicates that the erosion rate values of the mid-central rivers have no significant differences among them and occurs popularly with rate from moderate to strong. Specifically, the lateral migration occurs with moderate rate for Gianh

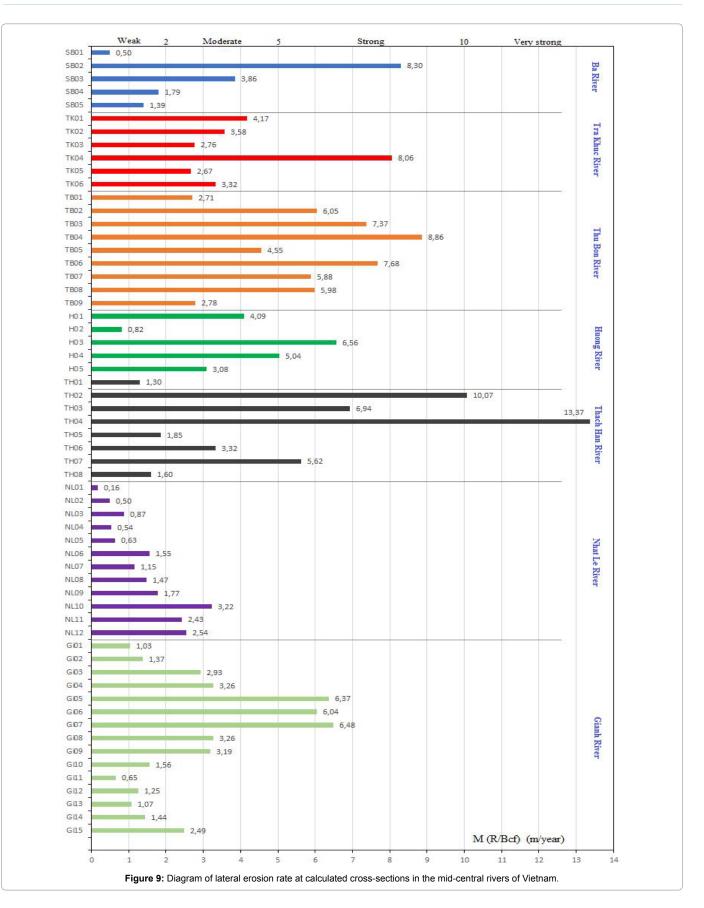
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River (2.85 m/y), Huong River (2.66 m/y), Tra Khuc River (3.30 m/y) and Ba River (2.35 m/y). Erosion activity of Thach Han River and Thu Bon River occurs with strong rate by 5.29 m/y and 5.62 m/y, respectively. In Nhat Le River, lateral erosion rate gets the lowest only 1.35 m/y. In addition, the maximum erosion rate of investigated rivers reaches 6.48-8.86 m/y even 13.37 (Thach Han), except Nhat Le River (3.32m/y). The minimum erosion rate raises from 0.16-1.3 m/y to 2.67-2.71 m/y for all of rives. These results are suitable for our field investigation and published researches in period 2012-2015 [13-15] (Figures 4-8 and Table 4) as well as the researches of other authors [1,28].

2. As shown in Tables 1 and 3 and Figures 4-9, the lateral migration activity of investigated rivers is strongly differentiated by space-time and depend completely on the morphological characteristics of river channel, soil composition and ground structure of riverbanks as well as hydrology - hydraulic regime of each river, especially river sections.

In which: Regarding to Gianh River, lateral erosion occurs with weak rate (0,65-1,56 m/y) in the middle stream (from Gi10-Gi14) and nearing estuary (from Gi01-Gi02) with the mean of 1.20 m/y. As for downstream of river (from Gi03-Gi09), this erosion process alternated in rate range from moderate (2,93-3,26 m/y, 3.03 m/y in mean) to strong (6,04-6,48 m/year, 6.30 m/y in mean). Although the high curvature ratio with value from 1,31 to 1,38, the riverbanks is structured from hard rocks get high erosion resistance lead to be less effected by lateral erosion. Specifically, the ground structure of riverbanks are mainly cohesive soils, granular soils with medium

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Rivers	Cross-sections of rivers	B <sub>cf</sub> (m)	$\overline{H_{cf}}$ (m)	R (m)	J <sub>cf</sub> (x10⁴)	Q <sub>cf</sub> (m³/s)	$\Omega_{cf}$ (N/m)	$\overline{S_{sb}}$ (N/m <sup>2</sup> )	M <sub>2.5</sub>	$\frac{R}{B_{cf}}$	$M(\frac{R}{B_{cf}})$ (m/y)
	Gi15	87	5.56	382	7.94	1063	8280	340	4.38	4.39	2.49
	Gi14	99	6.60	604	6.80	1093	7291	314	3.52	6.10	1.44
	Gi13	103	6.51	943	6.03	1105	6537	256	3.92	9.15	1.07
	Gi12	146	6.02	313	4.82	1146	5419	550	1.64	2.14	1.25
	Gi11	198	5.40	1400	4.21	1196	4939	498	1.84	7.07	0.65
	Gi10	248	7.12	1380	3.68	1690	6101	246	3.48	5.56	1.56
	Gi09	375	6.18	1994	3.48	1700	5804	138	6.80	5.32	3.19
	Gi08	325	6.07	1970	3.31	1700	5520	115	7.90	6.06	3.26
	Gi07	300	3.88	1682	2.98	1700	4970	88	14.55	5.61	6.48
	Gi06	450	5.95	1950	2.50	1700	4169	67	10.46	4.33	6.04
	Gi05	645	5.50	2750	2.15	1700	3585	60	10.86	4.26	6.37
	Gi04	500	5.24	4050	1.96	1300	2500	45	10.60	8.10	3.26
	Gi03	450	4.92	4475	1.79	1300	2283	40	11.60	9.94	2.93
	Gi02	497	8.86	4400	1.24	1310	1594	37	4.86	8.85	1.37
5	Gi01	399	8.90	4050	1.02	1310	1311	35	4.20	1015	1.03
	NL12	90	7.38	324	6.68	2110	13826	510	3.67	3.6	2.54
	NL11	137	6.32	287	6.03	2110	12481	590	3.35	2.09	2.43
	NL10	145	7.68	332	5.80	2120	12062	420	3.74	2.29	3.22
	NL09	141	7.24	943	4.21	2130	8796	256	4.75	6.69	1.77
	NL08	85	4.78	472	3.68	1410	5090	327	3.26	5.55	1.47
	NL07	51	3.25	313	3.41	1410	5073	550	2.84	6.13	1.15
	NL06	231	6.07	1380	2.75	1410	4717	210	3.70	5.97	1.55
5	NL05	426	5.85	1940	0.196	4020	773	115	1.15	4.55	0.63
	NL04	674	4.87	3100	0.185	2010	364	75	1.00	4.60	0.54
	NL03	752	4.45	2742	0.172	2010	339	60	1.27	3.65	0.87
5	NL02	556	4.64	4400	0.137	2020	271	37	1.58	7.91	0.50
	NL01	364	8.81	4050	0.111	2020	219	35	0.71	11.13	0.16
	TH08	130	5.37	1942	6.68	1750	11777	230	9.54	14.94	1.60
	TH07	249	4.54	1380	6.42	1750	11022	195	12.45	5.54	5.62
5	TH06	236	6.70	1625	5.57	1680	9180	150	9.13	6.89	3.32
	TH05	145	6.75	1760	4.24	1680	6988	115	9.00	12.14	1.85
	TH04	669	5.41	2750	3.71	2680	9754	82	21.99	4.11	13.37
	TH03	425	5.76	3652	3.45	2680	9070	66	23.86	8.59	6.94
	TH02	1209	5.02	4220	2.77	1350	3668	52	14.05	3.49	10.07
Ē	TH01	348	9.99	4050	1.96	1350	2596	43	6.04	11.64	1.30
	H05	173	7.20	2050	6.30	2550	15760	150	14.59	11.85	3.08
IAN RIONL	H04	206	7.22	1425	4.23	2550	10582	105	13.96	6.92	5.04
	H03	237	6.00	1057	2.61	2550	6529	93	11.70	4.46	6.56
Ŝ	H02	170	8.50	3580	1.57	2550	3927	67	6.90	21.06	0.82
	H01	371	3.74	3235	1.11	2550	2777	52	14.28	8.72	4.09
	ТВ09	395	5.85	1980	1.53	4350	6529	200	5.58	5.01	2.78
	TB08	280	4.91	1453	2.67	4350	11394	187	12.41	5.19	5.98
	TB07	295	6.29	1400	2.55	4350	10882	155	11.16	4.75	5.88
	TB06	390	5.37	1375	1.50	4350	6401	110	10.84	3.53	7.68
P	TB05	275	5.90	2557	2.34	4350	9986	100	16.92	9.30	4.55
	TB04	270	5.66	1100	1.82	4350	7767	95	14.44	4.07	8.86
5	TB03	350	5.45	1870	1.67	3250	5324	62	15.76	5.34	7.37
ב 5	TB02	747	8.80	2750	1.45	3250	4623	59	8.90	3.68	6.05
	TB01	365	7.55	3540	1.07	3250	3411	43	10.51	9.70	2.71
	TK06	500	3.38	2250	1.34	1400	1840	91	5.98	4.50	3.32
	TK05	340	4.41	2890	1.98	1400	2719	68	9.07	8.50	2.67
	TK04	640	1.96	2756	1.03	1400	1415	52	13.88	4.31	8.06
	ТК03	570	2.23	2540	0.53	1400	714	62	4.93	4.46	2.76
	TK02	870	1.99	3600	0.49	1400	673	66	5.93	4.14	3.58
	TK01	1550	2.85	3540	0.34	1400	467	60	3.81	2.28	4.17
	B05	230	17.23	1760	5.84	2100	12031	164	4.26	7.65	1.39
	B04	250	11.10	2750	4.75	2100	9785	112	7.87	11.00	1.79
Ē	B03	400	6.94	3652	4.04	2100	8323	85	14.11	9.13	3.86
Ba River	B02	400 550	4.57	4220	3.22	2100	6634	57	25.47	7.67	8.30
	B01	230	17.23	4050	1.27	2100	2616	43	3.53	17.61	0.50

**Table 1:** Results of determining rate of lateral erosion M (R/B<sub>r</sub>) in mid-downstream of research rivers.

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Rivers	Lateral erosion rate (m/y)						
	Min	Мах	Mean				
Gianh	0.65	6.48	2.85				
Nhat Le	0.16	3.22	1.35				
Thach Han	1.30	13.37	5.29				
Huong	0.82	6.56	2.66				
Thu Bon	2.71	8.86	5.62				
Tra Khuc	2.67	8.06	3.30				
Ва	0.50	8.30	2.35				

Table 2: The minimum, maximum and mean of lateral erosion rate in the investigated rivers (statistical analysis values).

Table 3: The mean of lateral erosion rate at each investigated river section.

Rivers	The mean of lateral erosion rate (m/y)							
	Weak <2 m/y	Moderate 2-5 m/y	Strong 5-10 m/y	Very strong >10 m/y				
Gianh	1.20	3.03	6.30	-				
Nhat Le	0.96	2.73	-	-				
Thach Han	1.58	3.32	6.28	11.72				
Huong	0.82	3.59	5.80	-				
Thu Bon	-	3.35	6.97	-				
Tra Khuc	-	3.30	8.06	-				
Ва	1.23	3.86	8.30	-				

Table 4: The assessment of erosion motivation in the mid-central rivers of Vietnam [13,15] (Li: Total length of the erosion sections).

Order	Rivers	River length (L, km)	Cofficient of erosion (K <sub>e</sub> =L/∑L <sub>i</sub> , %)	Erosion rate (V <sub>e</sub> ,m/s)	Rating motiation of river erosion
1	Gianh	80	16.0	2-5	Medium, harmful and serious
2	Nhat Le	57	9.7	1-2	Weak, less harmful, less serious
3	Thach Han	27	23.6	5-10	Strong, very harmful and very serious
4	Huong	40	18.0	2-5	Medium, harmful and serious
5	Thu Bon	55	26.9	5-10	Strong, very harmful and very serious
6	Tra Khuc	40	27.9	2-5	Medium, harmful and serious
7	Ва	50	25,6	2-5	Medium, harmful and serious

erosion resistance and be effected by high flood flows so that the erosion process occurred with rate from weak to moderate. The lateral erosion in Nhat Le River appeared with weak rate (0,16-1,77 m/y, 0.96 m/y in mean) with moving tendency commonly to the downstream the rate of lateral erosion decreased (at cross-section NL01-NL09). Specially in the middle stream (NL10-NL12), the riverbanks were created from hard rocks in mixture of clayey soils had relatively high erosion resistance, but they got totally effects of bottom forming flow lead to reaching level of lateral erosion moderate (2,43-3,22 m/year, 2.73 m/y in mean) in middle stream [5,23].

Due to meandering river channels and numerous anabranches, the flow velocity of Thach Han River changed complicated. The lateral erosion rate value has the alternation from weak (1,30-1,60 m/year, 1.58 m/y in mean) in the middle stream (at cross-section TH08) and estuary (TH01) to moderate (3,22 m/year - at cross-section TH06), strong (5,62-6,94 m/year, 6.28 m/y in mean; TH03, TH07) and very strong (10,07-13-37 m/year, 11.72 m/y in mean; TH02, TH04) in the downstream [3].

The lateral erosion rate of the Huong River has the partly change from the upper to downstream with specifically the moderate rate occurs at river cross-section H05 and H01 by 3,08-4,09 m/year and 3.59 m/year in mean. As for the middle stream, due to the curved river sections, the erosion occurs strongly with eroded values 5.04-6.56 m/year and mean value is 5.80 m/year at cross-section H04-H03. Especially, in the downstream, the erosion happens with the lowest rate by 0.82 m/year at H02 [7].

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The lateral erosion in mid-downstream of Thu Bon and Tra Khuc Rivers has features similar to alternative rates from moderate (2,67-4,55 m/year) to strong (5,88-8,86 m/year). In which, the lateral erosion occurs with moderate rate (Cross-sections TB09, TB01 in Thu Bon River and TK06, TK01, TK02, TK03 in Tra Khuc River) in the middle stream and nearing estuary parts. Because of curved river, appearance of large river sandbars, the flood flows are prevented. Therefore, the lateral erosion gets the alternative rate from moderate to strong and depends on hydrology - morphology characteristics of each river sections [11,15].

The erosion process of Ba Riverbank occurs with ascending rate from weak (1,39-1,79m/year, 1, 23 m/y in mean; B04-B05), moderate (3,86 m/year, B03) to strong (8,30 m/year, B02) in the way to downstream. At nearing estuary, due to low riverbanks, the flood spread out link to real bed forming discharge decline to 50% and weak lateral erosion [13,14].

#### Conclusion

From mentioned research results, we conclude and propose as following:

1. In whole research area, the rate of lateral migration rate alternates typical from moderate (Gianh River, Huong River, Tra Khuc River, Ba River) to strong (Thach Han River, Thu Bon River) with commonly tendency on the way to the downstream lateral erosion has decrease. In various rivers, as for Nhat Le River occurs weak lateral erosion.

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2. The lateral migration activity of investigated rivers is strongly differentiated by space-time and depend completely on the morphological characteristics of river channel, soil composition and ground structure of riverbanks as well as hydrology - hydraulic regime of each river, especially river sections.

3. The river channels of the mid - downstream in the research area get high slope, short, distributing nearly moderate mountains to follow orientation from the Northwest to Southeast. These are suitable conditions to hit from storm wind, moisture, which turned into the high rainfall zones, abundant water sources supply for the formation of flash floods, increasing intensity and scale of lateral erosion process in the mid-central rivers of Viet Nam.

4. The organic mud, cohesive soils, granular soils and gravels mainly structure the riverbanks. So, under the impact of bed forming discharge and economic - engineering activities (hydropower plants, bridges, roads, deforestation, sand - gravel exploitation), these river channels will still change in the flood season in next years.

5. The obtained outcomes of erosion rate calculating are quite consistent with our survey data and a number of other researches, which were cited in literatures. Especially, the rate values of lateral erosion at curved river sections get the highly reliability so that it is necessary to use for predicting the lateral migration for meandering rivers in the central part in particularly and for Vietnam in general.

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