



Peristaltic Flow in a non-Uniform Channel with Heat and Mass Transfer

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Abstract

The combined effect of heat and mass transfer on the peristaltic flow of fourth grade fluid in a non-uniform channel has been investigated. Flow analysis has been carried out in the presence of an induced magnetic field. The governing flow equations have been transformed in a wave frame. The arising equations have been solved for the stream function, pressure gradient, temperature, concentration, magnetic force function, induced magnetic field and current density. The role of embedded parameters is displayed and discussed.

Keywords

Induced magnetic field; Heat and mass transfer; Fourth grade fluid; Non-uniform channel

Introduction

The study of peristaltic mechanism has become popular among the researchers during the last four decades. This is because of its wide ranging industrial and physiological applications. In physiological processes it is used by the body to propel or mix the contents of the tube, for instance, in gastrointestinal tract, ureter, the bile duct, and other glandular ducts. Industrial use of peristaltic pumping in finger and roller pumps is quite obvious. Engineers adopted this processes to pump corrosive materials and fluids that must be kept away from pumping machinery. Further the transport of toxic liquid is met by the nuclear industry so as to not contaminate the environment [1]. Since the seminal work of Latham [2] several theoretical and experimental investigations have been carried out in order to understand the peristaltic flows of hydrodynamic fluids under varied assumptions of long wavelength, low Reynolds number, small wave amplitude etc. Although the literature on the topic is extensive but few recent investigations can be mentioned by the studies [3-10].

The peristaltic flows in the presence of magnetic field have also been examined. Agrawal and Anwaruddin [11] have studied the peristaltic flow of a blood under long wavelength and low Reynolds number assumption. Kothandapani and Srinivas [12] reported the peristaltic transport of a magnetohydrodynamic (MHD) Jeffrey fluid under the effect of magnetic field in an asymmetric channel. Mekheimer [13,14] and Hayat et al. [15] discussed the peristaltic flows of couple stress, micropolar and third grade fluids in the presence

of an induced magnetic field. Elmagboub [16] analyzed the induced magnetic field effect on the peristaltic flow in an annulus. Since most of the ducts in physiology are non-uniform so Pandey and Chaube [17] studied the peristaltic transport of a viscoelastic fluid in a tube of non-uniform cross section. Mekheimer [18] reported peristaltic flow of blood under effect of magnetic field in a non-uniform channel.

The interaction of peristalsis with heat and mass transfer is an important topic which has been given little attention so far. Srinivas et al. [19] investigated mixed convective peristaltic transport in an asymmetric channel. Srinivas and Muthuraj [20] presented peristaltic transport of a non-Newtonian fluid with chemical reaction and space porosity. Hayat et al. [21] discussed the role of heat transfer on the MHD peristaltic flow in a porous space. Kothandapani and Srinivas [22] have studied the influence of wall properties in the MHD peristaltic transport with heat transfer and porous medium. Ogulu [23] studied heat and mass transport of blood in a single lymphatic blood vessel with uniform magnetic field. Mekheimer and elmagboub [24] had reported the influence of heat transfer and magnetic field on peristaltic transport of Newtonian fluid in a vertical annulus. The influence of wall properties on the MHD peristaltic flow of a Maxwell fluid with heat and mass transfer in a symmetric channel has been investigated by Hayat and Hina.

The purpose of present research is to discuss the simultaneous effects of an induced magnetic field and heat and mass transfer on the peristaltic flow of a fourth grade fluid in a non-uniform channel. The considered fluid can predict the shear thinning/shear thickening effects. To the best of our knowledge, this problem has not been investigated yet. The paper is arranged as follows. Sections two and three provide the mathematical formulation and perturbed solution of the problem. Graphical discussion is presented in section four while the concluding remarks are given in section 5.

Formulation

An incompressible magneto hydrodynamic (MHD) fourth grade fluid in a non-uniform channel is considered. \bar{X} Axis is chosen in the direction of wave propagation and \bar{Y} transverse to it. A constant magnetic field of strength H_0 acts in the transverse direction which results in an induced magnetic field $\mathbf{H}(\bar{h}_{\bar{x}}(\bar{X}, \bar{Y}, \bar{t}), \bar{h}_{\bar{y}}(\bar{X}, \bar{Y}, \bar{t}), 0)$. The total magnetic field is $\mathbf{H}^+(\bar{h}_{\bar{x}}(\bar{X}, \bar{Y}, \bar{t}), H_0 + \bar{h}_{\bar{y}}(\bar{X}, \bar{Y}, \bar{t}), 0)$. The following expression describes the geometry of the channel wall

$$\bar{h}(\bar{X}, \bar{t}) = a(\bar{x}) + b \sin\left(\frac{2\pi}{\lambda}(\bar{X} - c\bar{t})\right) \quad (1)$$

With

$$a(\bar{x}) = a_0 + a_1 \bar{x}.$$

Here a_0 is half width at any inlet, ($a_1 \ll 1$) is constant, λ is the wavelength, a indicates the channel half width at any axial distance \bar{x} , b the wave amplitude, c the wave speed and t the time.

In fixed frame the fundamental equations governing the flow are

$$\nabla \cdot \mathbf{V} = 0 \quad (2)$$

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$$\begin{aligned} \frac{dV}{dt} &= \text{div } \mathbf{T} + \mu_e (\nabla \times \mathbf{H}^+) \times \mathbf{H}^+ \\ &= \text{div } \mathbf{T} + \mu_e \left[(\mathbf{H}^+ \cdot \nabla) \mathbf{H}^+ - \frac{\nabla \mathbf{H}^{+2}}{2} \right] \end{aligned} \quad (3)$$

$$\rho C_p \frac{dT}{dt} = \kappa \nabla^2 T + \mathbf{T} \cdot \mathbf{L}, \quad (4)$$

$$\frac{dC}{dt} = D \nabla^2 C + \frac{DK_T}{T_m} \nabla^2 T, \quad (5)$$

$$\frac{d\mathbf{H}^+}{dt} = \nabla \times (\mathbf{V} \times \mathbf{H}^+) + \frac{1}{\zeta} \nabla^2 \mathbf{H}^+ \quad (6)$$

in which $\zeta = \sigma \mu_e$ is the magnetic diffusivity, C_p the specific heat, T the temperature, D the coefficient of mass diffusivity, T_m the mean temperature, K_T the thermal diffusion ratio, C the concentration, K the thermal conductivity and the Cauchy stress tensor $\bar{\mathbf{T}}$ and extra stress tensor $\bar{\mathbf{S}}$ are

$$\bar{\mathbf{T}} = -p\bar{\mathbf{I}} + \bar{\mathbf{S}}, \quad (7)$$

$$\begin{aligned} \bar{\mathbf{S}} &= \mu \bar{\mathbf{A}}_1 + \alpha_1 \bar{\mathbf{A}}_2 + \alpha_2 \bar{\mathbf{A}}_3 + \beta_1 \bar{\mathbf{A}}_3 + \beta_2 (\bar{\mathbf{A}}_2 \bar{\mathbf{A}}_1 + \bar{\mathbf{A}}_1 \bar{\mathbf{A}}_2) + \beta_3 (\text{tr} \bar{\mathbf{A}}_2) \bar{\mathbf{A}}_1 + \gamma_1 \bar{\mathbf{A}}_4 \\ &+ \gamma_2 (\bar{\mathbf{A}}_3 \bar{\mathbf{A}}_1 + \bar{\mathbf{A}}_1 \bar{\mathbf{A}}_3) + \gamma_3 \bar{\mathbf{A}}_2^2 + \gamma_4 (\bar{\mathbf{A}}_2 \bar{\mathbf{A}}_1^2 + \bar{\mathbf{A}}_1^2 \bar{\mathbf{A}}_2) + \gamma_5 (\text{tr} \bar{\mathbf{A}}_2) \bar{\mathbf{A}}_2 + \\ &\gamma_6 (\text{tr} \bar{\mathbf{A}}_2) \bar{\mathbf{A}}_1^2 + \{ \gamma_7 \text{tr} \bar{\mathbf{A}}_3 + \gamma_8 \text{tr} (\bar{\mathbf{A}}_2 \bar{\mathbf{A}}_1) \} \bar{\mathbf{A}}_1. \end{aligned} \quad (8)$$

$$\bar{\mathbf{A}}_n = \frac{d\bar{\mathbf{A}}_n}{dt} + \bar{\mathbf{A}}_{n-1} (\text{grad} \bar{V}) + (\text{grad} \bar{V})^T \bar{\mathbf{A}}_{n-1}, \quad n > 1, \quad (9)$$

$$\bar{\mathbf{A}}_1 = (\text{grad} \bar{V}) + (\text{grad} \bar{V})^T, \quad (10)$$

Where $\alpha_i (i=1,2)$, $\beta_j (j=1-3)$ and $\gamma_k (k=1-8)$ are the material constants, $\bar{\mathbf{A}}_n$ the Rivlin-Ericksen tensors, d/dt the material derivative, μ the viscosity, λr the trace, T in the superscript is the matrix transpose, p the pressure and $\bar{\mathbf{I}}$ the identity tensor. The velocity $\bar{\mathbf{V}}$ for two-dimensional flow is of the form

$$\bar{\mathbf{V}} = [\bar{U}(\bar{X}, \bar{Y}, \bar{t}), \bar{V}(\bar{X}, \bar{Y}, \bar{t}), 0] \quad (11)$$

And the Maxwell's relations are

$$\nabla \cdot \mathbf{E} = 0, \quad \nabla \cdot \mathbf{H} = 0, \quad (12)$$

$$\nabla \times \mathbf{E} = -\mu_e \frac{\partial \mathbf{H}}{\partial t}, \quad \nabla \times \mathbf{H} = \mathbf{J}, \quad (13)$$

$$\mathbf{J} = \sigma (\mathbf{E} + \mu_e (\mathbf{V} \times \mathbf{H})) \quad (14)$$

in which \mathbf{J} , μ_e , σ , \mathbf{E} and \mathbf{H} represent the electric current density, the magnetic permeability, the electrical conductivity, the electric field and the magnetic field respectively.

The relations between the fixed frame (\bar{X}, \bar{Y}) and wave frame (\bar{x}, \bar{y}) can be written as

$$\begin{aligned} \bar{x} &= \bar{X} - c\bar{t}, & \bar{y} &= \bar{Y}, \\ \bar{u}(\bar{x}, \bar{y}) &= \bar{U} - c, & \bar{v}(\bar{x}, \bar{y}) &= \bar{V}. \end{aligned} \quad (15)$$

Here (\bar{U}, \bar{V}) and (\bar{u}, \bar{v}) depict the velocity components in the fixed and wave frames respectively. The two-dimensional equations in the wave frame are

$$\frac{\partial \bar{u}}{\partial \bar{x}} + \frac{\partial \bar{v}}{\partial \bar{y}} = 0, \quad (16)$$

$$\rho \left(\bar{u} + c \frac{\partial}{\partial \bar{x}} + \bar{v} \frac{\partial}{\partial \bar{y}} \right) \bar{u} + c \frac{\partial \bar{p}}{\partial \bar{x}} = \frac{\partial \bar{S}_{xx}}{\partial \bar{x}} + \frac{\partial \bar{S}_{yy}}{\partial \bar{y}} - \frac{\mu_e}{2} \left(\frac{\partial \bar{H}^{+2}}{\partial \bar{x}} \right) + \mu_e \left(\bar{h}_{\bar{x}} \frac{\partial \bar{h}_{\bar{x}}}{\partial \bar{x}} + \bar{h}_{\bar{y}} \frac{\partial \bar{h}_{\bar{y}}}{\partial \bar{y}} + H_0 \frac{\partial \bar{h}_{\bar{x}}}{\partial \bar{y}} \right), \quad (17)$$

$$\rho \left(\bar{u} + c \frac{\partial}{\partial \bar{x}} + \bar{v} \frac{\partial}{\partial \bar{y}} \right) \bar{v} + \frac{\partial \bar{p}}{\partial \bar{y}} = \frac{\partial \bar{S}_{yx}}{\partial \bar{x}} + \frac{\partial \bar{S}_{xy}}{\partial \bar{y}} - \frac{\mu_e}{2} \left(\frac{\partial \bar{H}^{+2}}{\partial \bar{y}} \right) + \mu_e \left(\bar{h}_{\bar{x}} \frac{\partial \bar{h}_{\bar{y}}}{\partial \bar{x}} + \bar{h}_{\bar{y}} \frac{\partial \bar{h}_{\bar{x}}}{\partial \bar{y}} + H_0 \frac{\partial \bar{h}_{\bar{y}}}{\partial \bar{y}} \right), \quad (18)$$

$$\rho C_p \left[\bar{u} + c \frac{\partial}{\partial \bar{x}} + \bar{v} \frac{\partial}{\partial \bar{y}} \right] \bar{T} = \kappa \left[\frac{\partial^2 \bar{T}}{\partial \bar{x}^2} + \frac{\partial^2 \bar{T}}{\partial \bar{y}^2} \right] + \bar{S}_{xx} \frac{\partial \bar{u}}{\partial \bar{x}} + \bar{S}_{yy} \frac{\partial \bar{v}}{\partial \bar{y}} + \bar{S}_{xy} \left(\frac{\partial \bar{u}}{\partial \bar{y}} + \frac{\partial \bar{v}}{\partial \bar{x}} \right), \quad (19)$$

$$\left[\bar{u} + c \frac{\partial}{\partial \bar{x}} + \bar{v} \frac{\partial}{\partial \bar{y}} \right] C = D \left[\frac{\partial^2 C}{\partial \bar{x}^2} + \frac{\partial^2 C}{\partial \bar{y}^2} \right] + \frac{DK_T}{T_m} \left[\frac{\partial^2 T}{\partial \bar{x}^2} + \frac{\partial^2 T}{\partial \bar{y}^2} \right] \quad (20)$$

We set the dimensionless quantities as

$$\begin{aligned} x &= \frac{\bar{x}}{\lambda}, \quad y = \frac{\bar{y}}{a_0}, \quad t = \frac{c\bar{t}}{\lambda}, \quad p = \frac{a_0^2 \bar{p}}{c\lambda\mu}, \quad M^2 = \text{Re} S^2 R_m, \quad \lambda_i = \frac{\alpha_i c}{\mu a_0} (i=1,2) \\ \delta &= \frac{a_0}{\lambda}, \quad S_{ij} = \frac{a_0 \bar{S}_{ij}}{\mu c} \quad (\text{for } i, j=1,2,3), \quad u = \frac{\bar{u}}{c}, \quad \eta_k = \frac{\gamma_k c^3}{\mu a_0^3} (k=1-8), \\ \text{Re} &= \frac{c a_0 \rho}{\mu}, \quad R_m = \sigma \mu_e a_0 c, \quad S = \frac{H_0}{c} \sqrt{\frac{\mu_e}{\rho}}, \quad \varphi = -\frac{\bar{\varphi}}{H_0 a_0}, \quad v = \frac{\bar{v}}{c}, \quad m = \frac{a_1}{a_0}, \\ \bar{h}_{\bar{x}} &= \frac{c a_0 \rho}{\mu} \bar{h}_{\bar{x}}, \quad \bar{h}_{\bar{y}} = -\bar{\varphi}_{\bar{x}}, \quad p_m = p + \frac{1}{2} \text{Re} \delta \frac{\mu_e (H^+)^2}{\rho c^2}, \quad E = \frac{-\bar{E}}{c H_0 \mu_e}, \quad \gamma = \frac{\bar{T} - T_0}{T_0}, \\ \text{Pr} &= \frac{\mu C_p}{\kappa}, \quad \Omega = \frac{C - C_0}{C_0}, \quad \xi_j = \frac{\beta_j c^2}{\mu a_0} (j=1,2,3). \end{aligned} \quad (21)$$

In above definitions P_r , δ , Re , R_m , S and M denote the Prandtl, wave, Reynolds, magnetic Reynolds, Stommer's and Hartman numbers respectively and the total pressure p_m is sum of ordinary and magnetic pressures, E the electric field strength, m the non-uniformity parameter, γ the temperature, Ω the concentration and φ the magnetic force function. Further T_0 and C_0 denote the temperature and concentration at $y=h$.

Equation (1) in dimensionless form reduces to

$$h = \frac{\bar{h}}{a_0} = 1 + mx + \alpha \sin(2\pi x), \quad (22)$$

In which the amplitude ratio α is equal to b/a_0 .

Putting

$$u = \frac{\partial \Psi}{\partial \bar{y}}, \quad v = -\delta \frac{\partial \Psi}{\partial \bar{x}}, \quad h_x = \frac{\partial \varphi}{\partial \bar{y}}, \quad h_y = -\delta \frac{\partial \varphi}{\partial \bar{x}} \quad (23)$$

Equations (2) automatically satisfied and equations (3-20) can be easily arranged as

$$\begin{aligned} \text{Re} \delta \left(\frac{\partial \Psi}{\partial \bar{y}} \frac{\partial}{\partial \bar{x}} - \frac{\partial \Psi}{\partial \bar{x}} \frac{\partial}{\partial \bar{y}} \right) \frac{\partial \Psi}{\partial \bar{y}} + \frac{\partial p_m}{\partial \bar{x}} = \delta \frac{\partial S_{xx}}{\partial \bar{x}} + \frac{\partial S_{xy}}{\partial \bar{y}} + \delta \text{Re} S^2 \left(\frac{\partial \varphi}{\partial \bar{y}} \frac{\partial}{\partial \bar{x}} - \frac{\partial \varphi}{\partial \bar{x}} \frac{\partial}{\partial \bar{y}} \right) \frac{\partial \varphi}{\partial \bar{y}} \\ + \text{Re} S^2 \frac{\partial^2 \varphi}{\partial \bar{y}^2}, \end{aligned} \quad (24)$$

$$\text{Re} \delta^2 \left(\frac{\partial \Psi}{\partial \bar{y}} \frac{\partial}{\partial \bar{x}} - \frac{\partial \Psi}{\partial \bar{x}} \frac{\partial}{\partial \bar{y}} \right) \frac{\partial \Psi}{\partial \bar{x}} + \frac{\partial p_m}{\partial \bar{y}} \quad (25)$$

$$= \delta \left(\delta \frac{\partial S_{yx}}{\partial \bar{x}} + \frac{\partial S_{yy}}{\partial \bar{y}} \right) - \delta^3 \text{Re} S^2 \left(\frac{\partial \varphi}{\partial \bar{y}} \frac{\partial}{\partial \bar{x}} - \frac{\partial \varphi}{\partial \bar{x}} \frac{\partial}{\partial \bar{y}} \right) \frac{\partial \varphi}{\partial \bar{x}} - \text{Re} \delta^2 S^2 \frac{\partial^2 \varphi}{\partial \bar{x} \partial \bar{y}},$$

$$\begin{aligned} \text{Re} \delta \left(\frac{\partial \Psi}{\partial \bar{y}} \frac{\partial}{\partial \bar{x}} - \frac{\partial \Psi}{\partial \bar{x}} \frac{\partial}{\partial \bar{y}} \right) \gamma = E_1 \left\{ \delta (S_{xx} - S_{yy}) \frac{\partial^2 \Psi}{\partial \bar{x} \partial \bar{y}} + S_{xy} \left(\frac{\partial^2 \Psi}{\partial \bar{y}^2} - \delta^2 \frac{\partial^2 \Psi}{\partial \bar{x}^2} \right) \right\} \\ + \frac{1}{\text{Pr}} \left(\delta^2 \frac{\partial^2 \varphi}{\partial \bar{x}^2} + \frac{\partial^2 \varphi}{\partial \bar{y}^2} \right) \gamma, \end{aligned} \quad (26)$$

$$-\text{Re} \delta \left(\frac{\partial \Psi}{\partial \bar{y}} \frac{\partial}{\partial \bar{x}} - \frac{\partial \Psi}{\partial \bar{x}} \frac{\partial}{\partial \bar{y}} \right) \Omega = \frac{1}{Sc} \left(\delta^2 \frac{\partial^2 \varphi}{\partial \bar{x}^2} + \frac{\partial^2 \varphi}{\partial \bar{y}^2} \right) \Omega + Sr \left(\delta^2 \frac{\partial^2 \varphi}{\partial \bar{x}^2} + \frac{\partial^2 \varphi}{\partial \bar{y}^2} \right) \gamma, \quad (27)$$

$$E = \frac{\partial \Psi}{\partial \bar{y}} - \delta \left(\frac{\partial \Psi}{\partial \bar{y}} \frac{\partial \varphi}{\partial \bar{x}} - \frac{\partial \Psi}{\partial \bar{x}} \frac{\partial \varphi}{\partial \bar{y}} \right) + \frac{1}{R_m} \left(\delta^2 \frac{\partial^2 \varphi}{\partial \bar{x}^2} + \frac{\partial^2 \varphi}{\partial \bar{y}^2} \right) \varphi, \quad (28)$$

Where, the subscripts depict the partial differentiation. Adopting the long wavelength and low Reynolds number procedure we obtain

$$\frac{\partial p}{\partial x} = \frac{\partial S_{xy}}{\partial y} + Re S^2 \frac{\partial^2 \varphi}{\partial y^2}, \tag{29}$$

$$\frac{\partial p}{\partial y} = 0, \tag{30}$$

$$\frac{1}{Pr} \frac{\partial^2 \gamma}{\partial y^2} + E_1 S_{xy} \frac{\partial^2 \Psi}{\partial y^2} = 0, \tag{31}$$

$$\frac{1}{Sc} \frac{\partial^2 \Omega}{\partial y^2} + Sr \frac{\partial^2 \gamma}{\partial y^2} = 0, \tag{32}$$

$$E = \frac{\partial \Psi}{\partial y} + \frac{1}{R_m} \frac{\partial^2 \varphi}{\partial y^2} \tag{33}$$

With the subjected boundary conditions

$$\Psi = 0, \quad \frac{\partial^2 \Psi}{\partial y^2} = 0, \quad \frac{\partial \varphi}{\partial y} = 0 \quad \text{at } y = 0,$$

$$\Psi = F, \quad \frac{\partial \Psi}{\partial y} = -1, \quad \varphi = 0 \quad \text{at } y = h, \tag{34}$$

$$\frac{\partial \gamma}{\partial y} = 0, \quad \frac{\partial \Omega}{\partial y} = 0, \quad \text{at } y = 0,$$

$$\gamma = 0, \quad \Omega = 0, \quad \text{at } y = h,$$

where $p \neq p(y)$ and F is the dimensionless time mean flow rate in the wave frame which can be related to dimensionless time mean flow rate θ in the laboratory frame by $\theta = F + 1$,

$$F = \int_0^h \frac{\partial \Psi}{\partial y} dy. \tag{35}$$

From Equation (8) (29) and (30) we obtain

$$\frac{\partial p}{\partial x} = \frac{\partial}{\partial y} \left[\Psi_{,yy} \left\{ 1 + 2\Gamma \left(\frac{\partial^2 \Psi}{\partial y^2} \right)^2 \right\} \right] + M^2 \left(E - \frac{\partial \Psi}{\partial y} \right) \tag{36}$$

$$\frac{\partial^4 \Psi}{\partial y^4} + 2\Gamma \frac{\partial^2}{\partial y^2} \left(\frac{\partial^2 \Psi}{\partial y^2} \right)^3 - M^2 \frac{\partial^2 \Psi}{\partial y^2} = 0, \tag{37}$$

Where $\Gamma = \xi_2 + \xi_3$ is used for the Deborah number.

Perturbation Solution Writing

$$\begin{aligned} \Psi &= \Psi_0 + \Gamma \Psi_1 + \dots \\ F &= F_0 + \Gamma F_1 + \dots \\ p &= p_0 + \Gamma p_1 + \dots \\ \varphi &= \varphi_0 + \Gamma \varphi_1 + \dots \\ \gamma &= \gamma_0 + \Gamma \gamma_1 + \dots \\ \Omega &= \Omega_0 + \Gamma \Omega_1 + \dots \end{aligned} \tag{38-43}$$

And inserting into Equations (31, 32, 34, 36, and 37) we get the zero and first order systems. Solving the resulting zero and first order systems one obtains

$$\begin{aligned} \psi &= \frac{B_0}{6M^2} (\cosh(4My) - \sinh(4My)) C_1(y) \\ &+ \Gamma \left[\frac{B_0^4 M^4}{120M^8} (\cosh(4My) - \sinh(4My)) \sum_{i=2}^7 C_i(y) \right], \end{aligned} \tag{44}$$

$$\begin{aligned} \frac{dp}{dx} &= B_0 M^2 [(1 - FM) - (\cosh(2Mh) + \sinh(2Mh))(1 + F)] \\ &+ \Gamma \left[\frac{B_0^3 M^6 (F + h)^3}{120} \sum_{j=1}^3 L_j(y) \right], \end{aligned} \tag{45}$$

$$\begin{aligned} \varphi &= \frac{R_m}{2M} (\cosh(My) - \sinh(My)) B_1(y) \\ &+ \Gamma \left[\frac{R_m M^3 B_0^5 (F + h)^4}{480} (\cosh(4My) - \sinh(4My)) \sum_{k=2}^6 B_k(y) \right], \end{aligned} \tag{46}$$

$$\begin{aligned} \gamma &= \frac{1}{4} (\cosh(2My) - \sinh(2My)) A_1(y) \\ &+ \Gamma \left[\frac{BrM^6 B_0^4 (F + h)^4}{18000} (\cosh(5My) - \sinh(5My)) \sum_{l=2}^8 A_l(y) \right] \end{aligned} \tag{47}$$

$$\begin{aligned} \Omega &= \frac{1}{4} (\cosh(2My) - \sinh(2My)) A_9(y) \\ &+ \Gamma \left[\frac{BrM^6 B_0^4 (F + h)^4}{18000} (\cosh(5My) - \sinh(5My)) \sum_{l=9}^{16} A_l(y) \right] \end{aligned} \tag{48}$$

Where the values of the involved $A_l (l=1-16)$, $B_k (k=0-6)$, $C_i (i=1-7)$ and $L_j (j=1-3)$ can be given through algebraic computations and $F_0 = F - \Gamma F_1$ has been used in the above expressions. To save space we avoid to present the values of A_p , B_k , C_i and L_j here.

The definitions of dimensionless axial induced magnetic field h_x , current density J_z and pressure rise ΔP_λ are

$$h_x = \frac{\partial \varphi}{\partial y} \tag{49}$$

$$J_z = -\frac{\partial h_x}{\partial y} \tag{50}$$

$$\Delta P_\lambda = \int_0^1 \left(\frac{dp}{dx} \right)_{y=0} dx \tag{51}$$

Graphical Results and Discussion

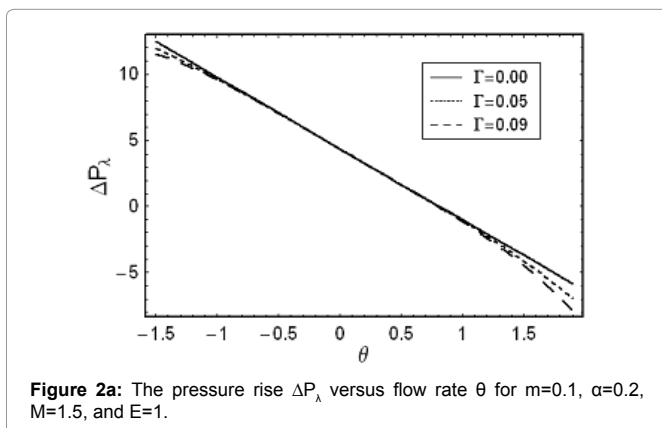
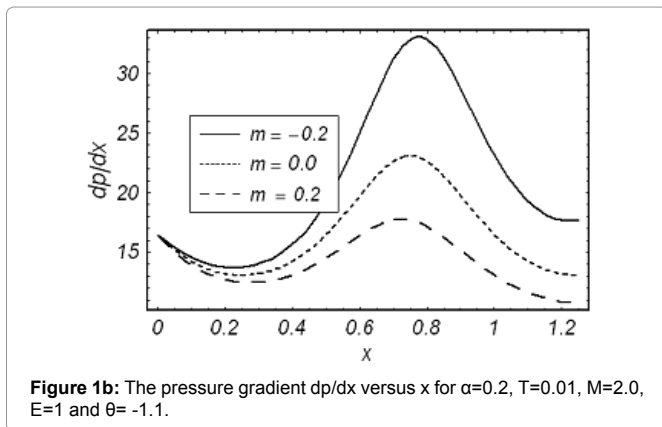
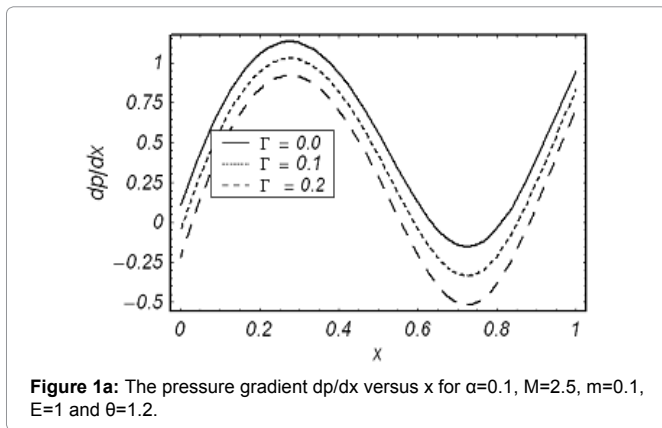
In this section we present the effects of various parameters (i.e., material parameter Γ non-uniformity parameter m , Hartman number M , Brinkman number Br and Schmidt number Sc) on the temperature γ , current density J_z , axial induced magnetic field h_x , pressure gradient dp/dx , pressure rise ΔP_λ and axial velocity μ . Hence Figures 1-6 have been displayed.

Pumping characteristics

Figures 1a and 1b presents the axial pressure gradient dp/dx with x when different values of Γ and m are accounted. It is seen in Fig. 1a that amplitude of dp/dx decreases with an increase in Γ . Figure 1b elucidates that dp/dx for a divergent channel ($m > 0$) is higher when compared to uniform channel ($m = 0$) On the other hand dp/dx is lowest for a convergent channel ($m < 0$).

The pressure rise ΔP_λ against the flow rate θ is sketched in Figure 2a, 2b. Pumping action divides the region into four sections: Pumping region ($\Delta p_\lambda > 0, \theta > 0$) augmented pumping ($\Delta p_\lambda < 0, \theta > 0$) retrograde pumping ($\Delta p_\lambda > 0, \theta < 0$) and free pumping ($\Delta p_\lambda = 0$).

The pressure rise ΔP_λ for different values of Γ is shown in Figure 2a. It is noticed that pumping rate decreases by increasing Γ however for certain values of flow rate the pumping curves coincide which indicate that there is no difference between the Newtonian and fourth grade fluids. The pressure rise ΔP_λ for convergent channel is also larger in magnitude when compared with the straight and divergent channels (Figure 2b).



Flow characteristics

The performed analysis shows that axial velocity at the wall ($u(y=h)=-1$) satisfies the no-slip boundary condition for all values of the parameters. The parametric presentation near the channel walls is different from the behavior at the center of channel. The velocity μ for different values of Γ is shown in Figure 3a. We observed that the velocity profile increases with an increase in Γ . Figure 3b illustrates the effects of m on u . Velocity for divergent channel is larger in magnitude in comparison to the straight and convergent channels at $y=0$.

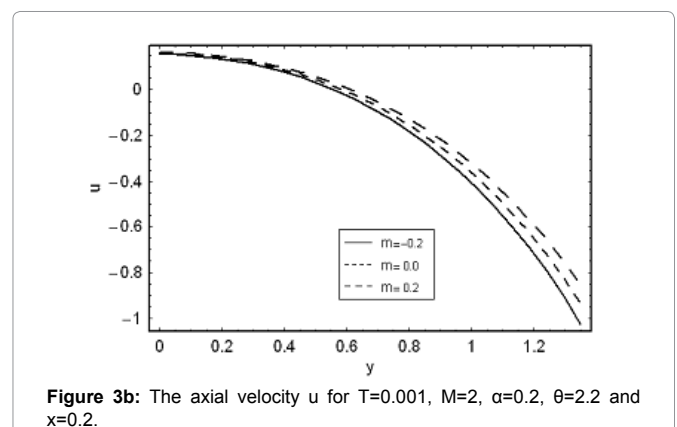
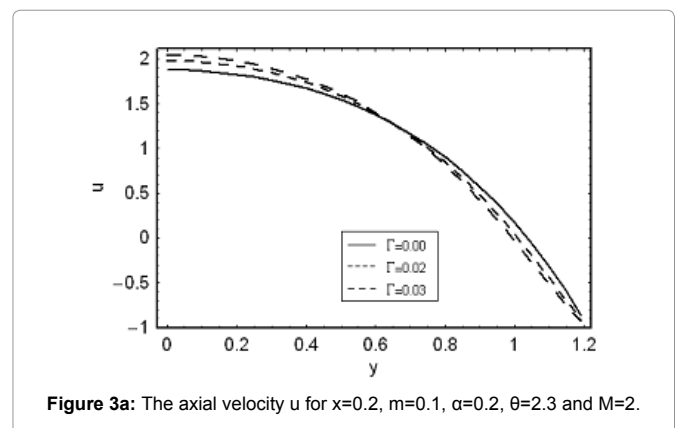
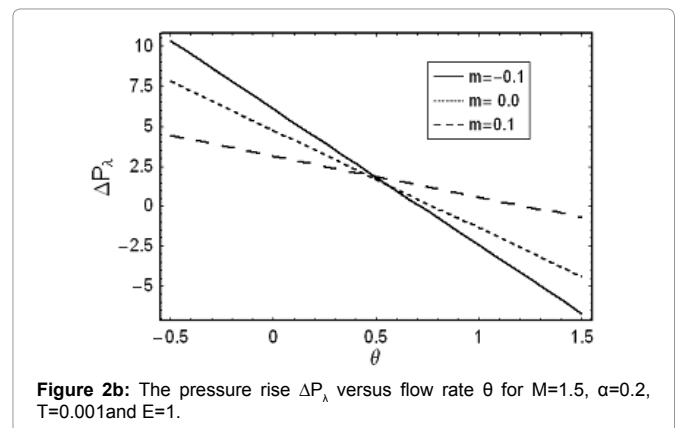
Magnetic field characteristics

The axial induced magnetic field h_x and the current density distribution J_z across the channel for various values of Γ and m are

displayed in the Figures 4a and 4b) and Figures 5a and 5b respectively. The prominent features of induced magnetic field are as follows. In the half region of the channel, the induced magnetic field is in one direction whereas it is in the opposite direction in the other half region. It is zero at $y=0$ which is compatible with the imposed boundary condition.

Figure 4a indicates the variation of axial induced magnetic field h_x against y for the various values of Γ . It is found that magnitude of h_x increases with Γ . Figure 4b Depicts that an induced magnetic field h_x for divergent channel is largest in magnitude.

We have constructed Figures 5a and 5b just to see the variation of current density distribution J_z within y for the different values of Γ



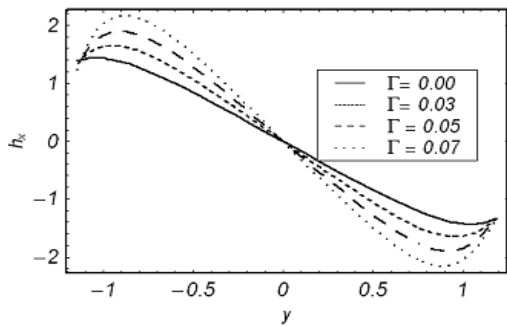


Figure 4a: The axial induced magnetic field h_x versus y for $M=4.5$, $\theta=3.5$, $X=0.2$, $\alpha=0.2$, $R_m=1$, $m=0.1$ and $E=1$.

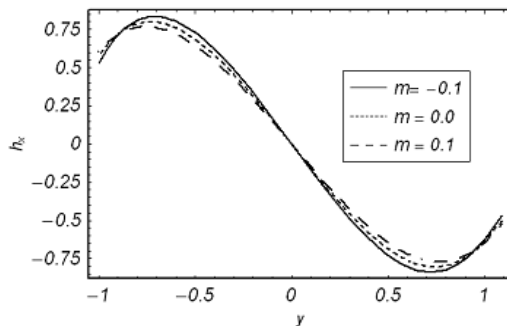


Figure 4b: The axial induced magnetic field h_x versus y for $M=1.5$, $\theta=2.5$, $X=0.2$, $\alpha=0.2$, $R_m=1$, $T=0.1$ and $E=1$.

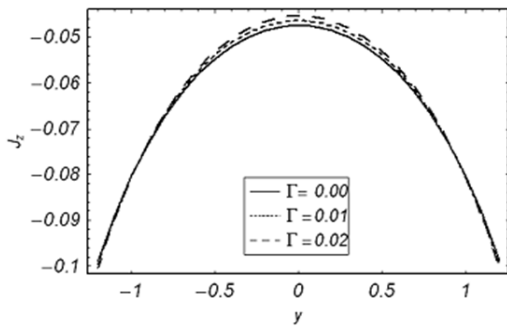


Figure 5a: Current density J_z versus y for $M=1.5$, $\theta=1.2$, $x=0.2$, $m=0.1$, $\alpha=0.8$, $R_m=0.1$ and $E=1$.

and m Obviously the graphs of current density are parabolic in nature. Behavior of parameters at the center of channel is quite different from near the walls of channel.

The current density distribution J_z within y for various values of Γ have been plotted in Figure 5a. It is observed that magnitude of J_z decreases when Γ increases at the Centre of channel while it increases range of y near the channel walls. The behavior of J_z against y for the different values of m is shown in Figure 5b. This Fig. depicts that magnitude of J_z increases as we move from convergent to divergent channel at $y=0$.

Temperature characteristics

Here we analyze the salient features of Γ, M, m and Br on temperature distribution. Keeping such in mind, Figures 6a-6d have

been sketched. Clearly the temperature distribution is an increasing function of Γ and Br . Hartman number M has an increasing effect on y when $y=0$. However y decreases near the walls of channel (Figure 6b). Figure 6c elucidates that the temperature for a convergent channel ($m < 0$) is lower when compared with uniform channel ($m = 0$). The temperature distribution is highest for a divergent channel ($m < 0$).

Concentration characteristics

The variation of concentration field Ω with y for various values of Γ, M, m and Br and Sc are discussed in this section. It is worth noting that concentration profiles show quite opposite behavior than temperature distribution. Concentration field is a decreasing function of Γ, Br and Sc (Figures 7a, 7d and 7e). It is clear from Figure 7b that

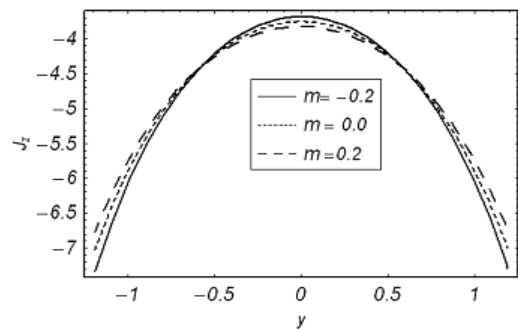


Figure 5b: Current density J_z versus y for $T=0.001$, $\theta=2.5$, $x=0.2$, $M=0.1$, $\alpha=0.2$, $R_m=1$ and $E=6$.

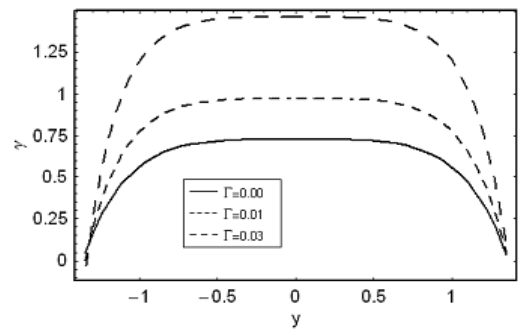


Figure 6a: The temperature distribution Y versus y for $M=1.5$, $\theta=3$, $x=0.1$, $\alpha=0.2$, $m=0.1$ and $Br=0.2$.

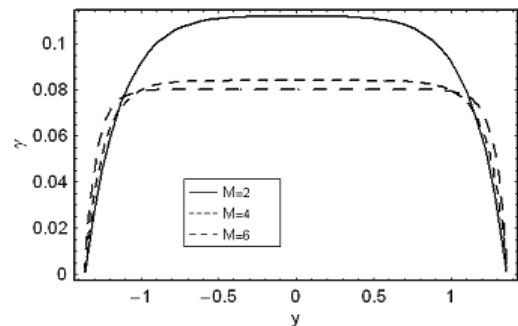


Figure 6b: The temperature distribution Y versus y for $T=0.01$, $\theta=1$, $x=0.1$, $\alpha=0.6$, $m=0.1$ and $Br=0.2$.

Hartman number M has direct proportionality with concentration field at $y=0$. However, the situation is quite opposite near the walls. Figure 7c indicates concentration field is highest for the convergent channel in comparison to straight and divergent channels.

Concluding Remarks

The peristaltic flow of fourth grade fluid has been examined in a non-uniform channel. Analysis is presented when an induced magnetic field, heat, and mass transfer effects have been accorded. The main observations have been summarized below.

- Both pressure gradient and pressure rise are smaller for the divergent channel ($m > 0$).

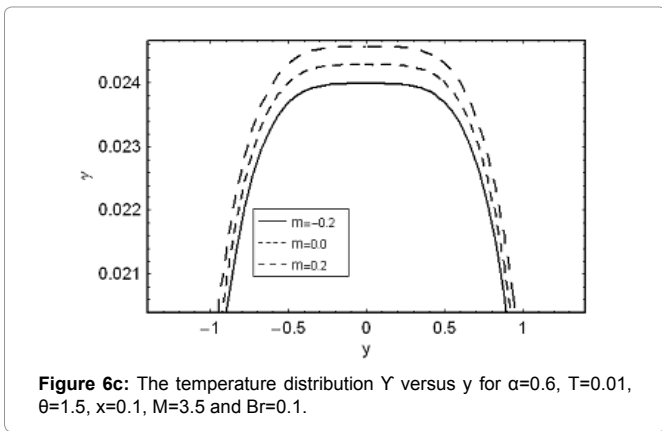


Figure 6c: The temperature distribution Y versus y for $\alpha=0.6$, $T=0.01$, $\theta=1.5$, $x=0.1$, $M=3.5$ and $Br=0.1$.

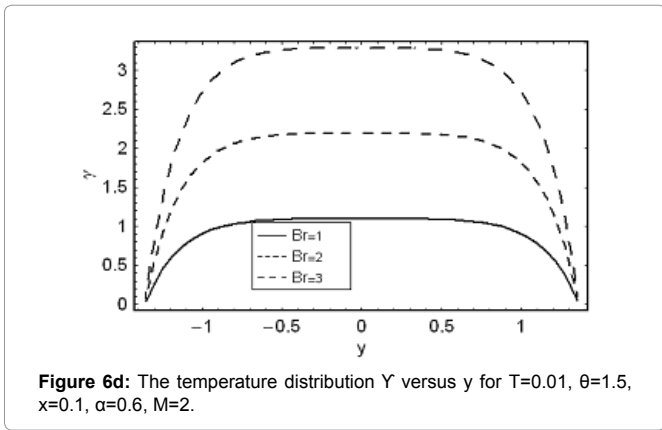


Figure 6d: The temperature distribution Y versus y for $T=0.01$, $\theta=1.5$, $x=0.1$, $\alpha=0.6$, $M=2$.

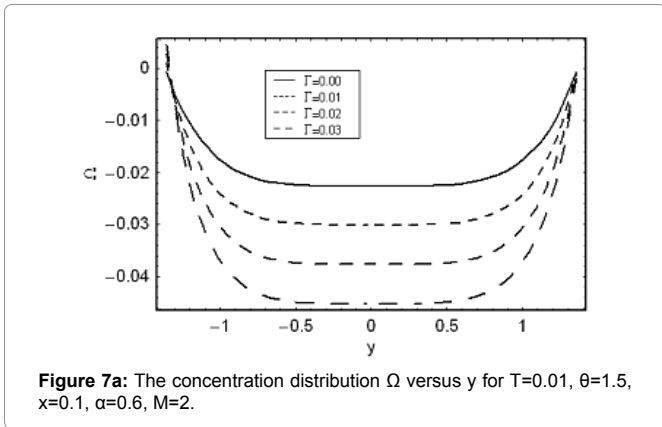


Figure 7a: The concentration distribution Ω versus y for $T=0.01$, $\theta=1.5$, $x=0.1$, $\alpha=0.6$, $M=2$.

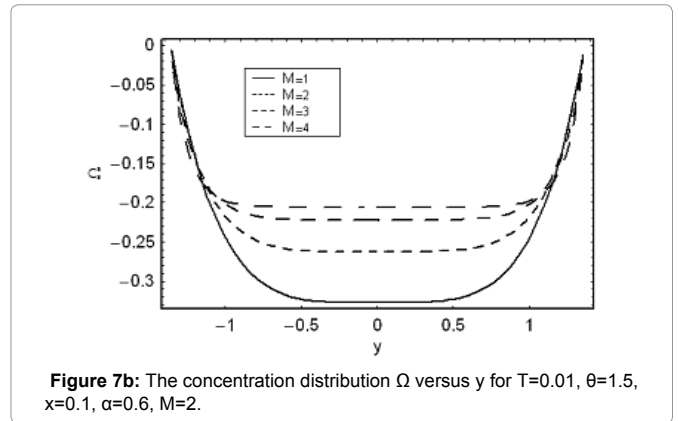


Figure 7b: The concentration distribution Ω versus y for $T=0.01$, $\theta=1.5$, $x=0.1$, $\alpha=0.6$, $M=2$.

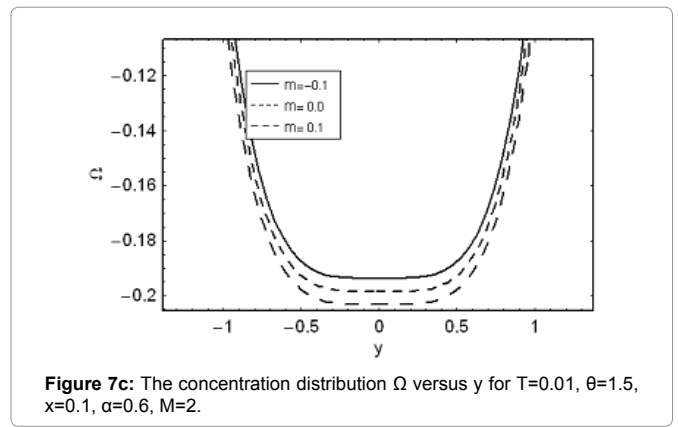


Figure 7c: The concentration distribution Ω versus y for $T=0.01$, $\theta=1.5$, $x=0.1$, $\alpha=0.6$, $M=2$.

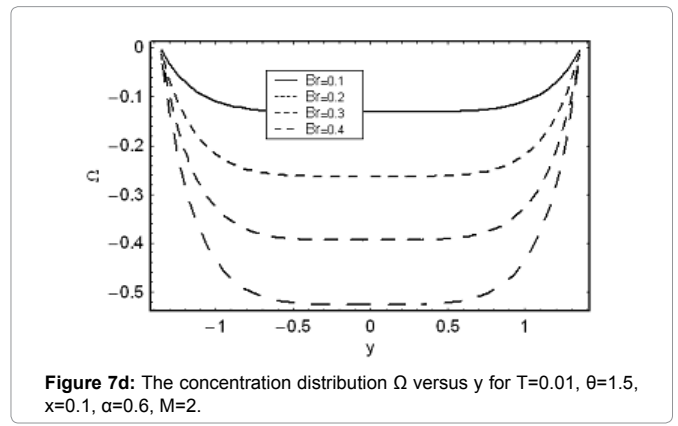


Figure 7d: The concentration distribution Ω versus y for $T=0.01$, $\theta=1.5$, $x=0.1$, $\alpha=0.6$, $M=2$.

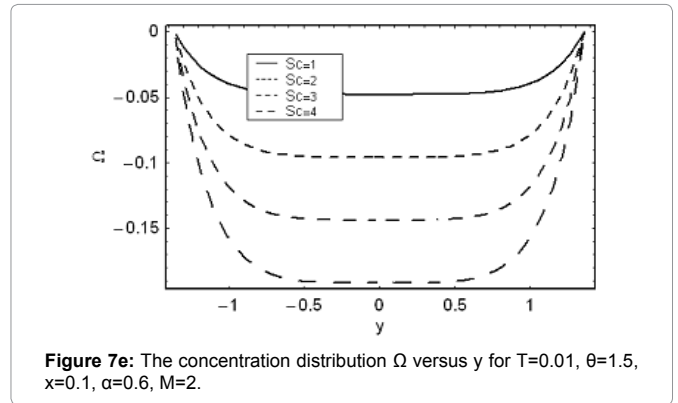


Figure 7e: The concentration distribution Ω versus y for $T=0.01$, $\theta=1.5$, $x=0.1$, $\alpha=0.6$, $M=2$.

- Pressure gradient and pressure rise are decreasing functions of Γ .
- The magnitude of velocity is an increasing function of Γ at the Centre line of the channel.
- Magnitude of induced magnetic field decreases with m .
- The magnitude of current density profiles has a decreasing effect for Γ .
- The temperature distribution increases with increasing values of Γ, M and Br near the walls of channel.
- The concentration field is an increasing function of M and decreasing function of Sc, Γ and Br when $y=0$.
- Magnitude of γ and Ω is larger for divergent channel ($m=0$) in comparison to straight channel ($m=0$) and convergent channel ($m=0$).

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